

Coastal hydrodynamics and morphodynamics

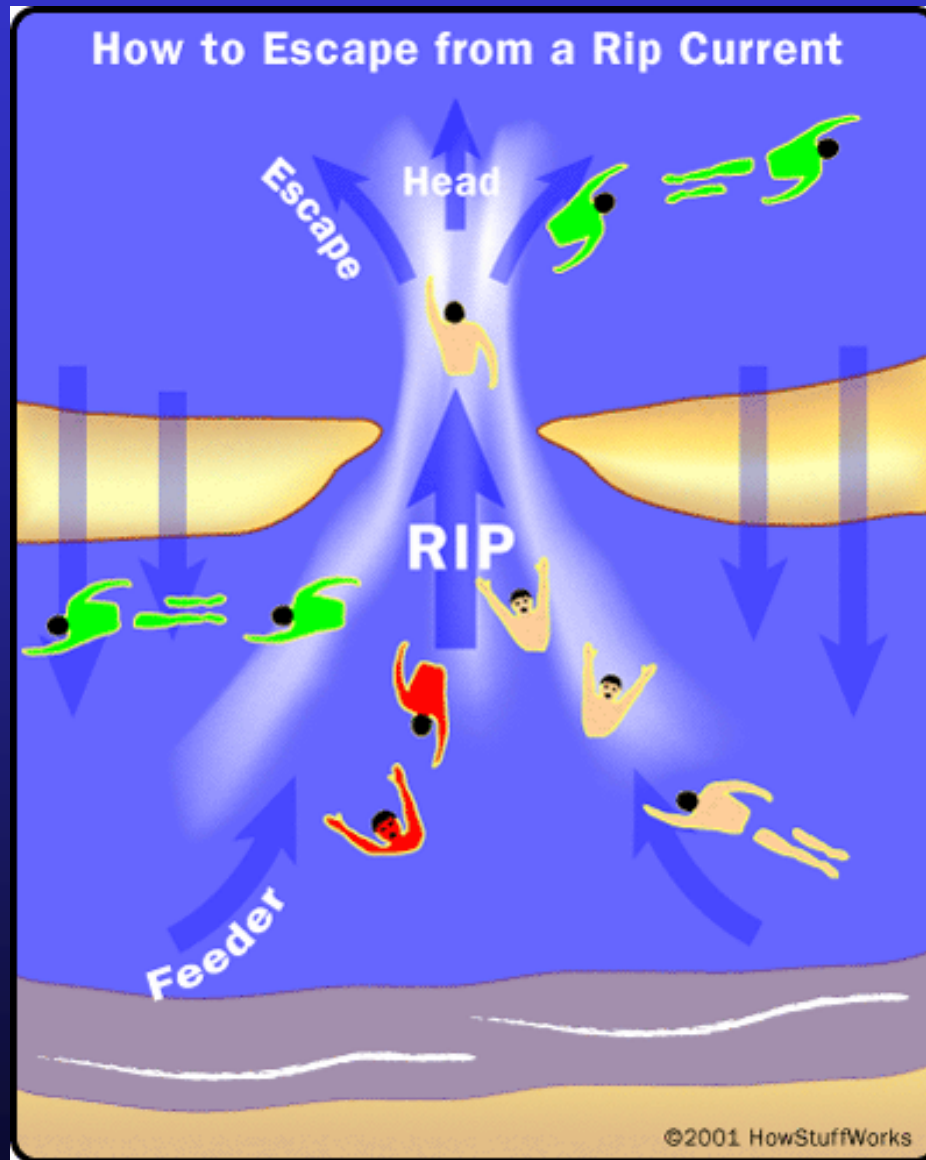


H.E. de Swart (IMAU, Utrecht Univ., the Netherlands)

JMBC Course Granular Matter, February 2008

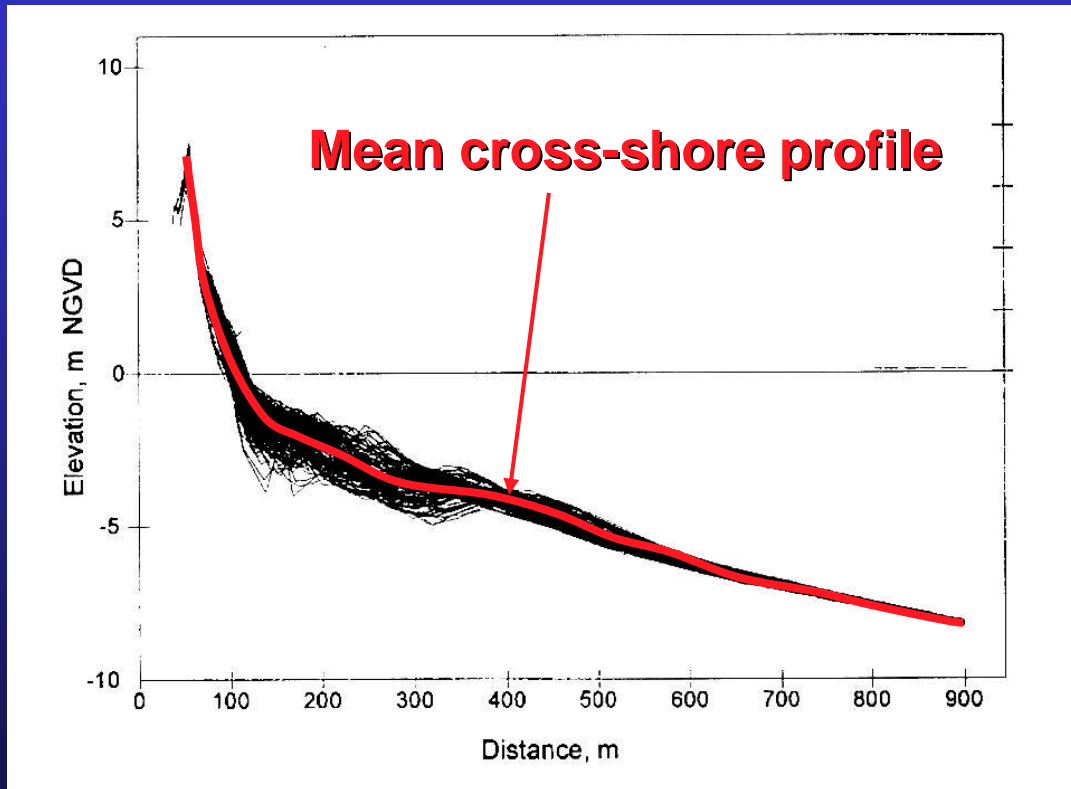


Rip currents cause many casualties each year



Many sandy coasts are characterized by

- **mean cross-shore bottom profile**
(mean = alongshore + time-average)



Duck (NC)

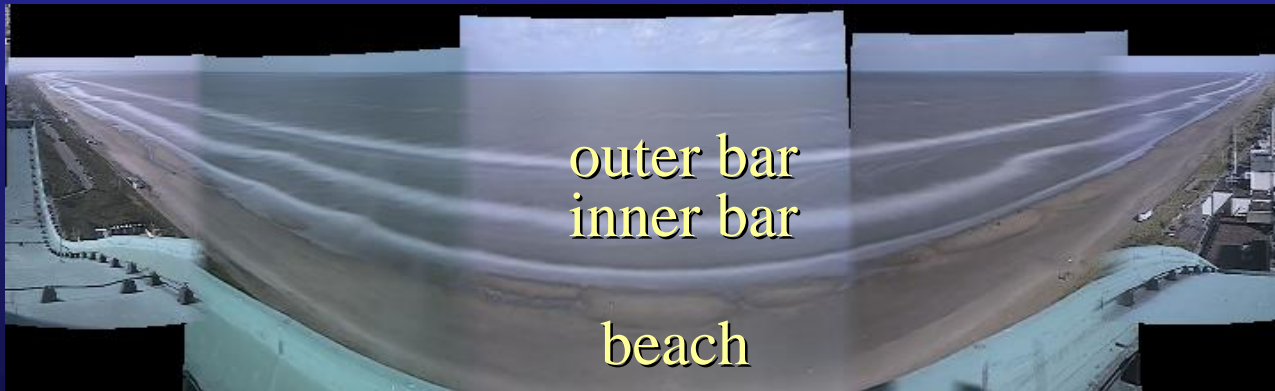
+ rhythmic bottom patterns
(cross-shore/longshore)

'Non-trivial' / rhythmic topography :

Example 1: longshore bars in the surf zone



ARGUS video system



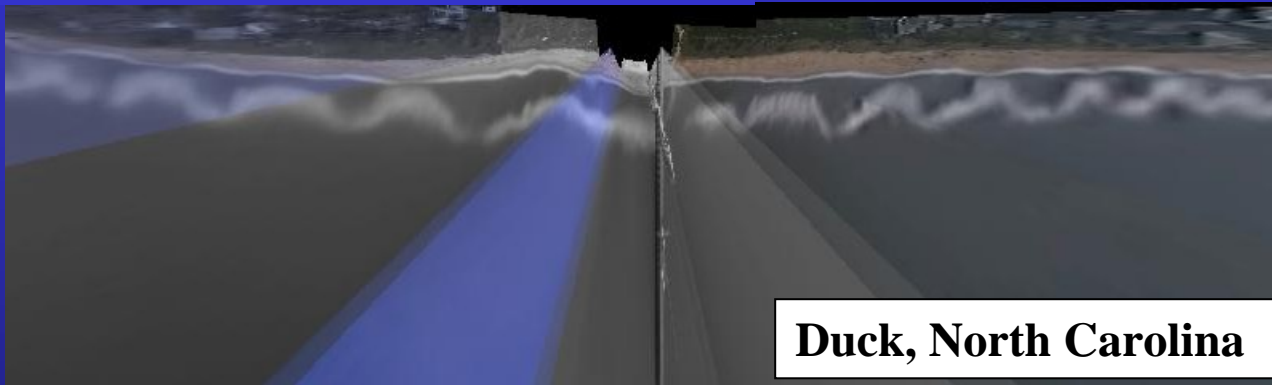
panorama image
Noordwijk

Cross-shore length scale ~ 100 m
Generation timescale ~ years

Example 2: rhythmic bar patterns in the surf zone

Many complex patterns are alongshore rhythmic:

Crescentic bar and rip channels



Duck, North Carolina

Shore-oblique bars

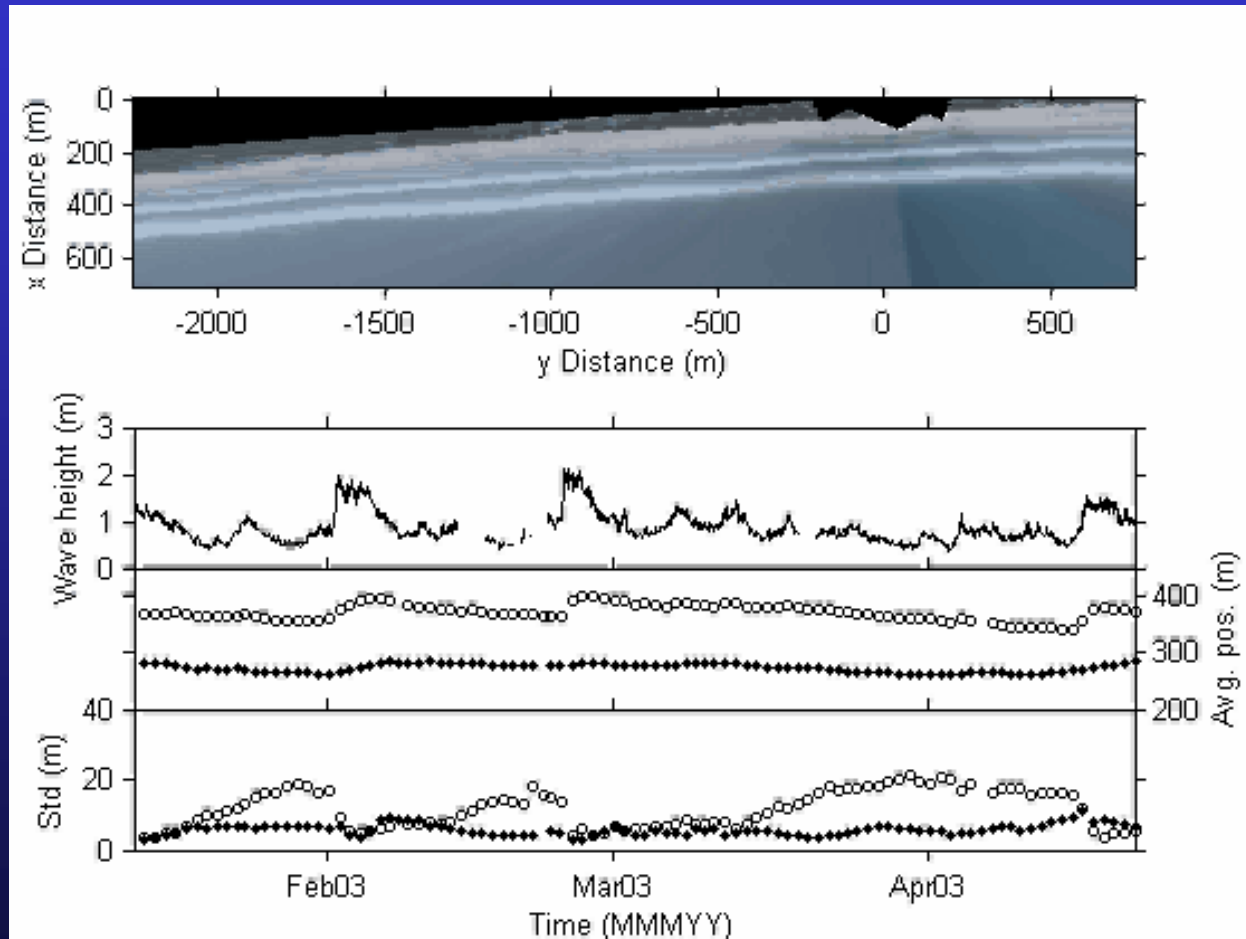


Truc Vert Beach,
Atlantic French Coast

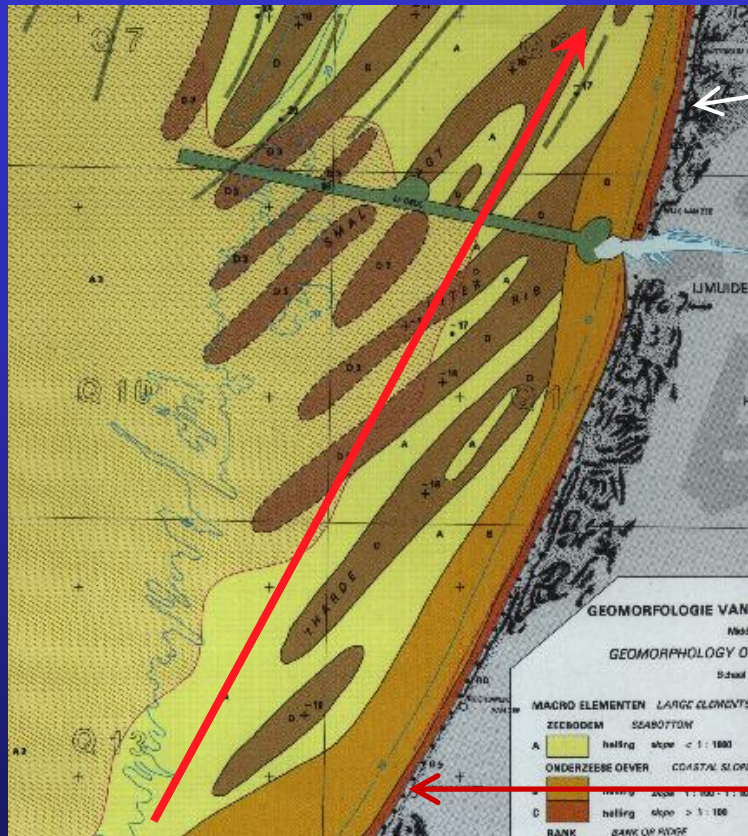
alongshore length scales:
~ 100 - 1000 m

time scale: days - weeks

Variability of sand banks (Gold Coast, Australia)



Example 3: shoreface-connected ridges on the inner shelf



Egmond

bathymetric map
Dutch coastal zone

red arrow : direction
of storm-driven flow

Noordwijk

- ridges observed in depths of 10-20 m
- alongshore length scale: ~ 5 km
- migrate northward: ~ 2 m/yr
- heights: 1-6 m
- crests: 'upcurrent' orientation
- time scale: centuries

Objectives of this presentation:

1. Discuss models that yield fundamental knowledge about

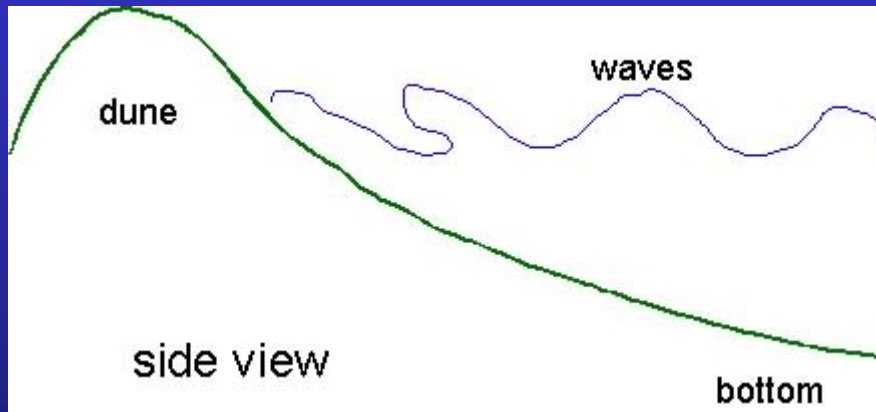
- stability properties of equilibrium beach profiles
(<- > formation of bars and sand ridges)
- characteristics of bars and ridges
(time scale, migration, spatial pattern, grain sorting)
- finite-amplitude behaviour (saturation?)

2. tools to address practical problems, e.g.

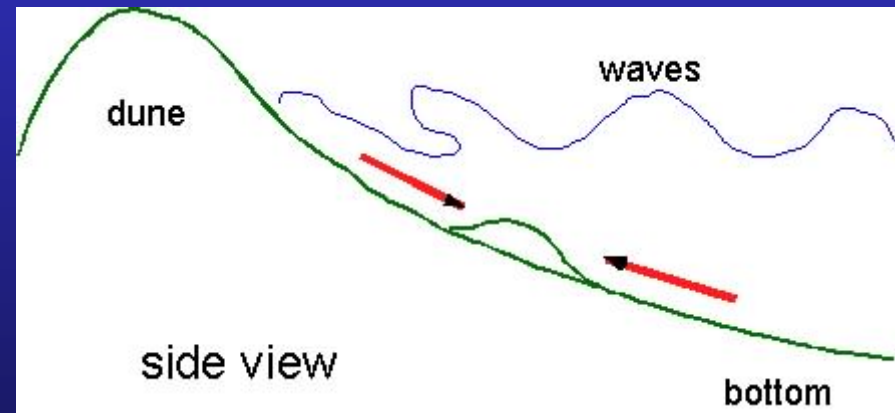
- **morphodynamic response to large-scale human interventions**
(e.g. sand mining, dredging navigation channels,
beach nourishment, construction of harbors, seawalls...)
-

Main message:

formation of many bars/ridges is due to self-organization
(i.e., inherent instabilities of the coupled water-bottom system)



equilibrium



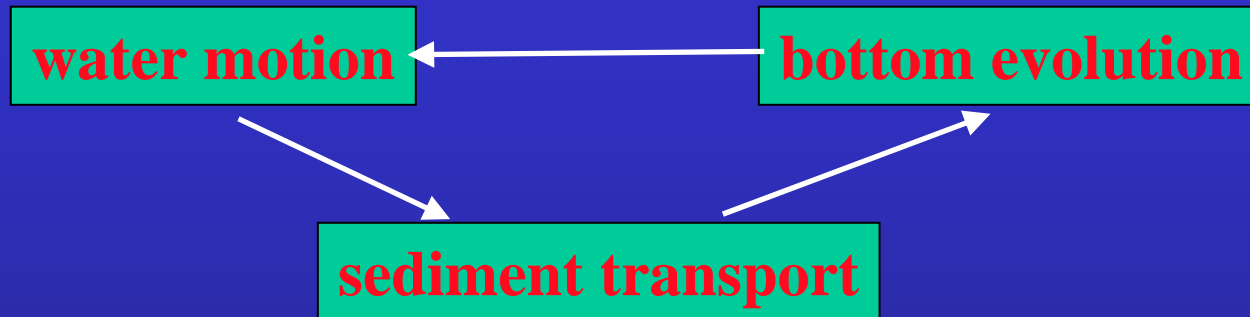
perturbation =>

**net sediment flux (red arrows)
here positive feedback: growth**

**spatial/temporal scales of bars/ridges
uncorrelated with external forcing**

Procedure:

1. Formulation of a model :



Here: idealized = straight coast, forcing alongshore uniform
limited number of physical processes + simplified description

2. Find an equilibrium state

3. Perform linear stability analysis

dynamics of small perturbations, arbitrary scales, do they grow?

Each perturbation -> growth rate

mode with the largest growth rate: the preferred mode
=> spatial pattern, migration speed, growth time scale

4. Perform nonlinear (stability) analysis

finite-amplitude behaviour of bars and ridges

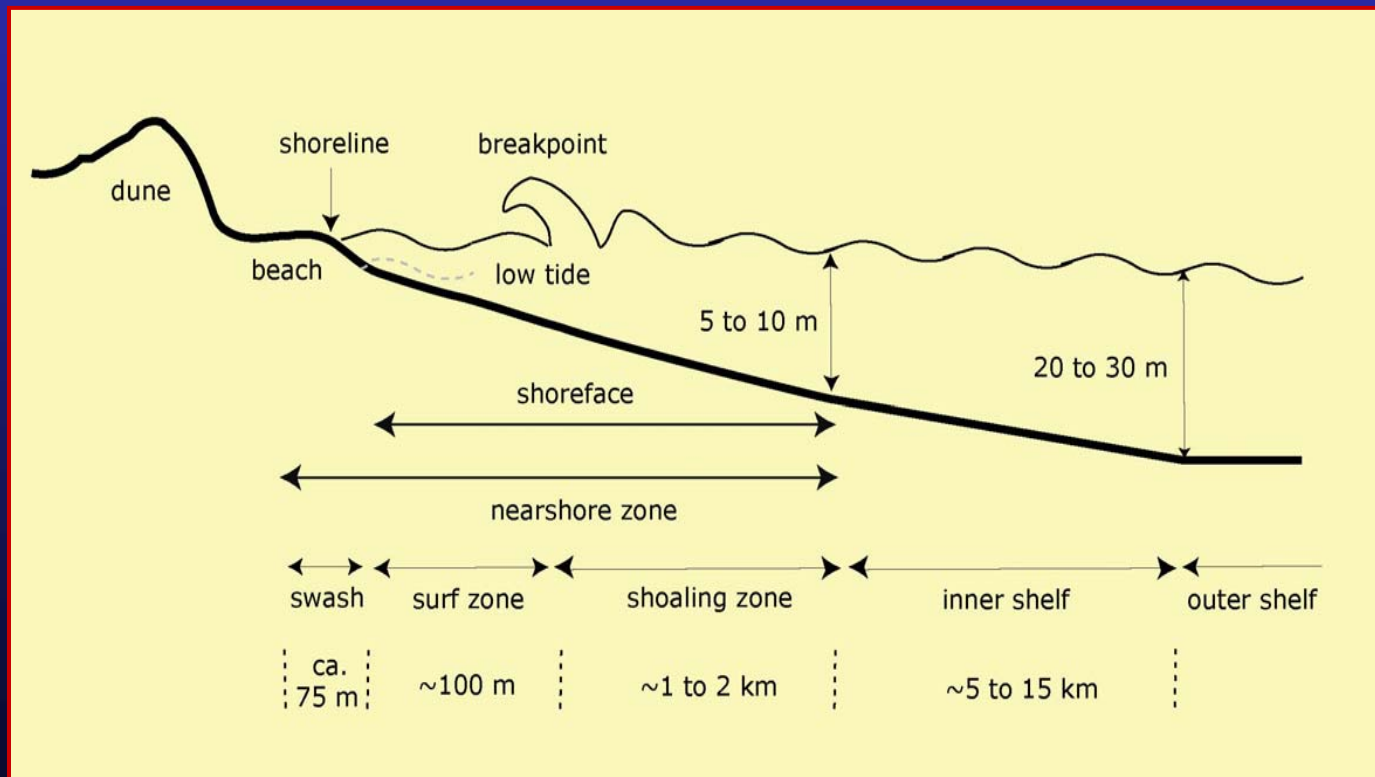
Forthcoming topics:

A. Inner shelf dynamics

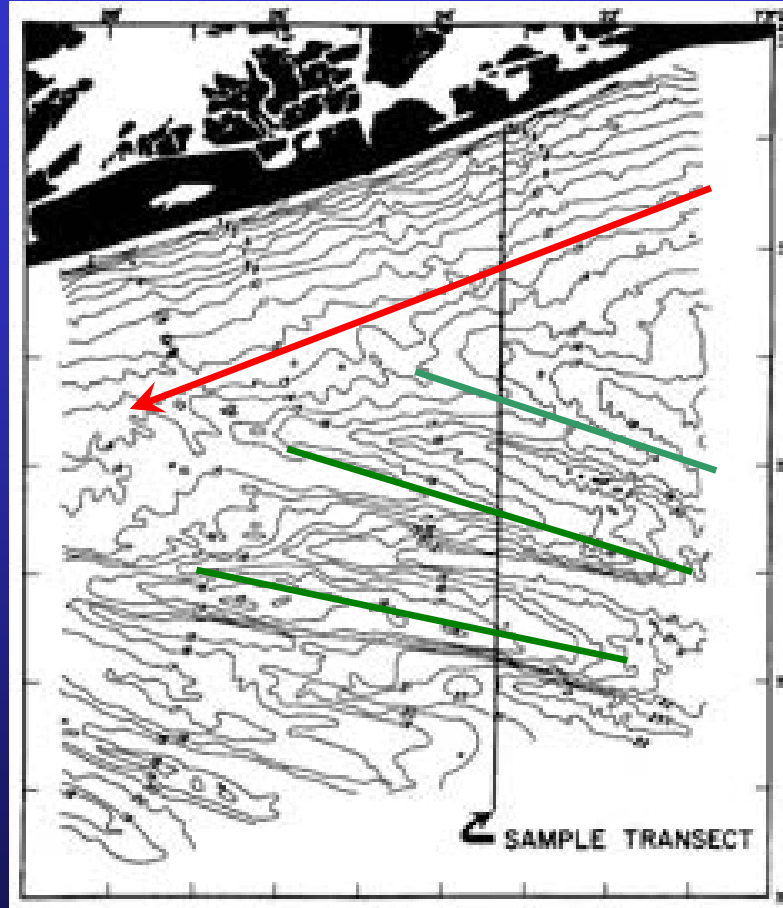
(shoreface-connected ridges: formation and saturation)

B. Surf zone dynamics (very brief)

(alongshore rhythmic bars: formation and saturation)



Topic A: shoreface-connected sand ridges (sfcrr)



Long Island (USA)

ridges: green lines

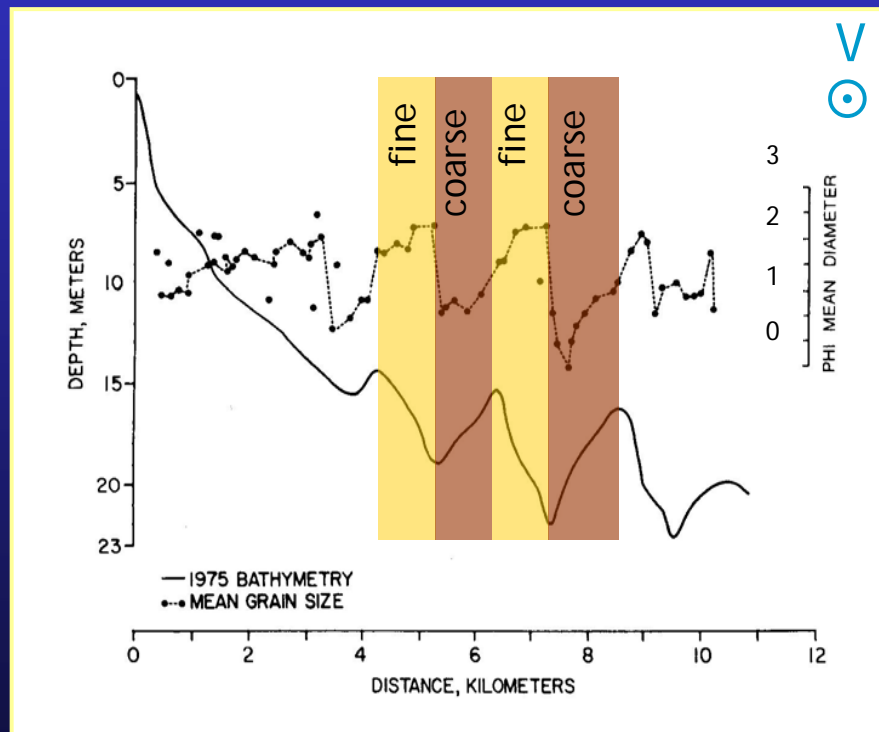
red arrow: direction
of storm-driven flow

1. Initial formation
2. Finite-amplitude behaviour
3. Response to interventions

Field observations reveal:

persistent variations in mean grain size over sfc

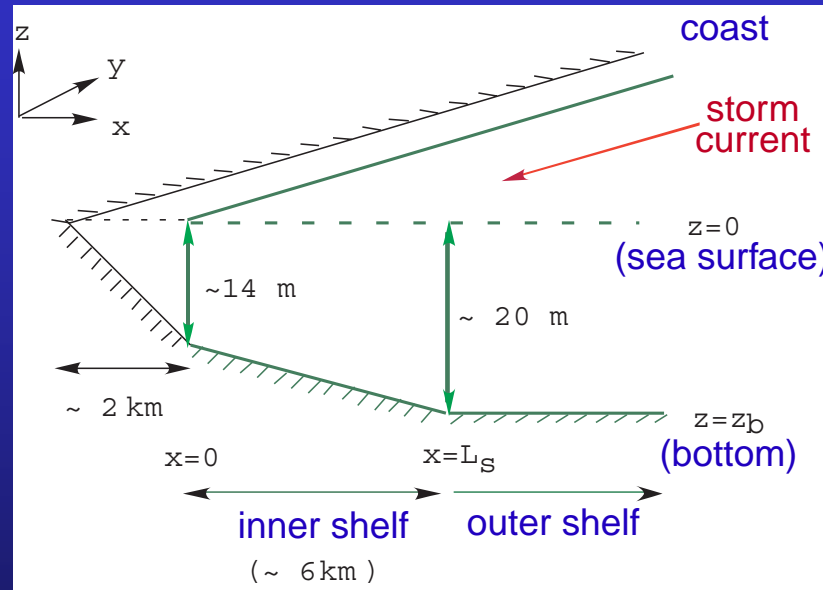
Profile of water depth and mean grain size



finest sediment (largest phi) seaward of the crests

Initial formation and physical mechanism

Trowbridge (1995): sfcr can form as free morphodynamic instabilities in a coupled water - bottom system:

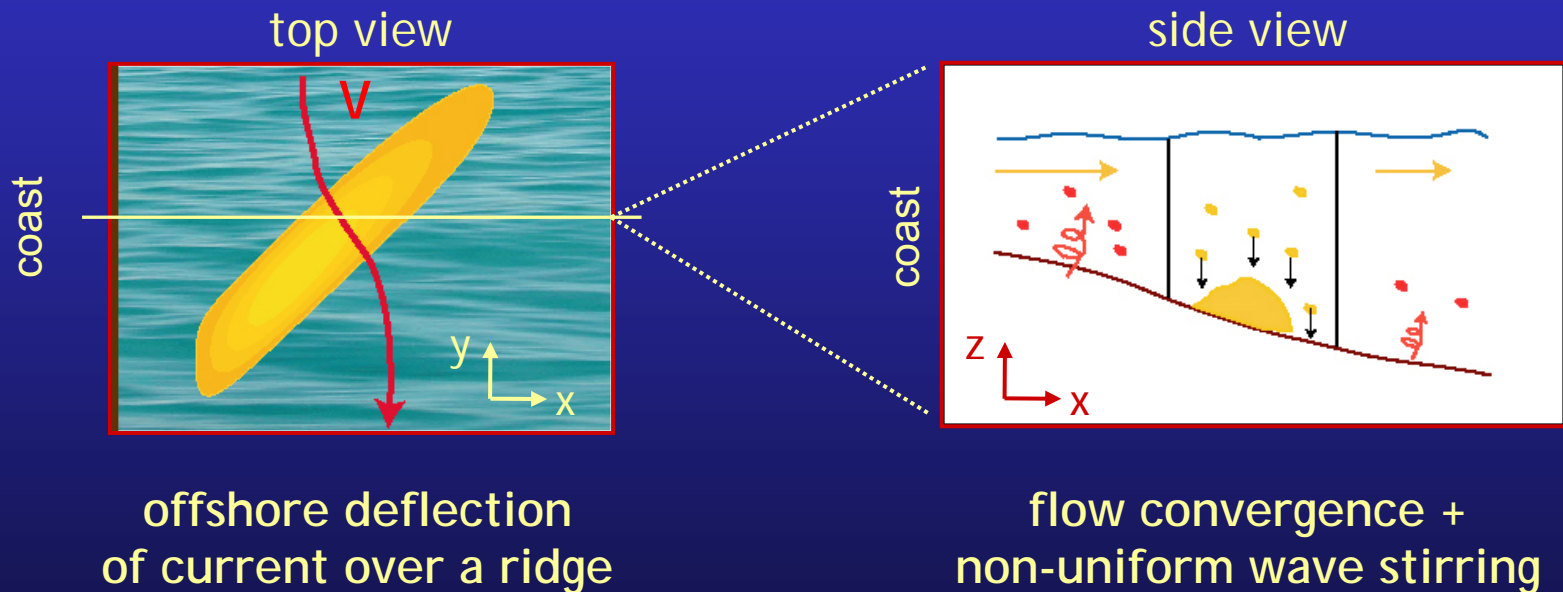


geometry

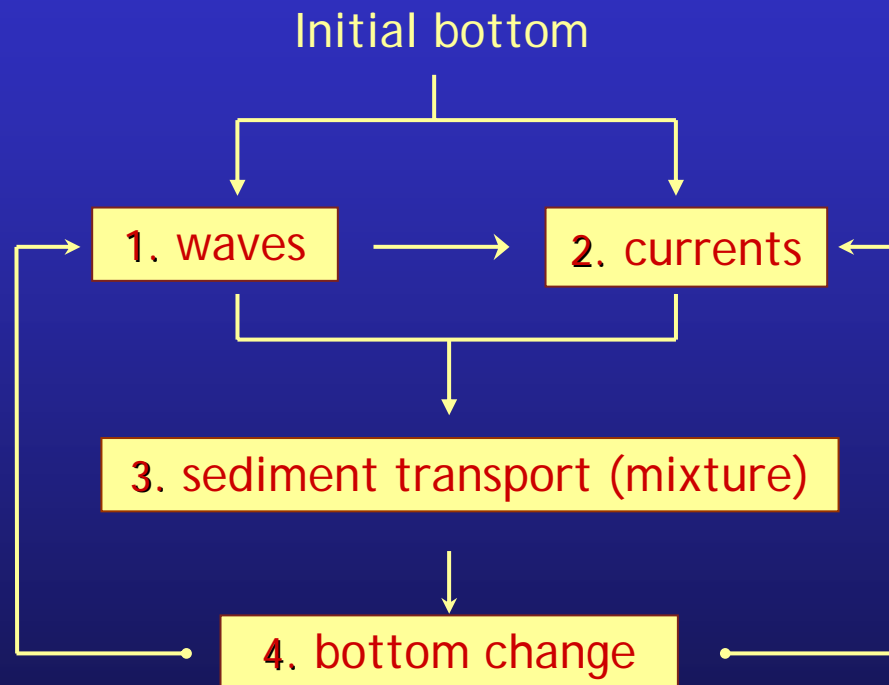
- Water motion: depth-averaged shallow water equations
- Sediment transport: stirring by waves, transport by currents
i.e., bedload formulation $\vec{q} = K \vec{u}$
- Instability \sim transverse bottom slope of the shelf

Instability mechanism

~ transverse bottom slope



Formulation of the model



dynamics only during storms (5%)

Wave model

- Dispersion relation
- Conservation of wave crests
- Generalised Snell law
- Energy balance
- Dissipation: bottom friction

$$\sigma^2 = g\kappa \tanh(\kappa D)$$

$$\frac{\partial \vec{\kappa}}{\partial t} + \vec{\nabla} \sigma = 0$$

$$\frac{\partial k}{\partial y} = \frac{\partial l}{\partial x}$$

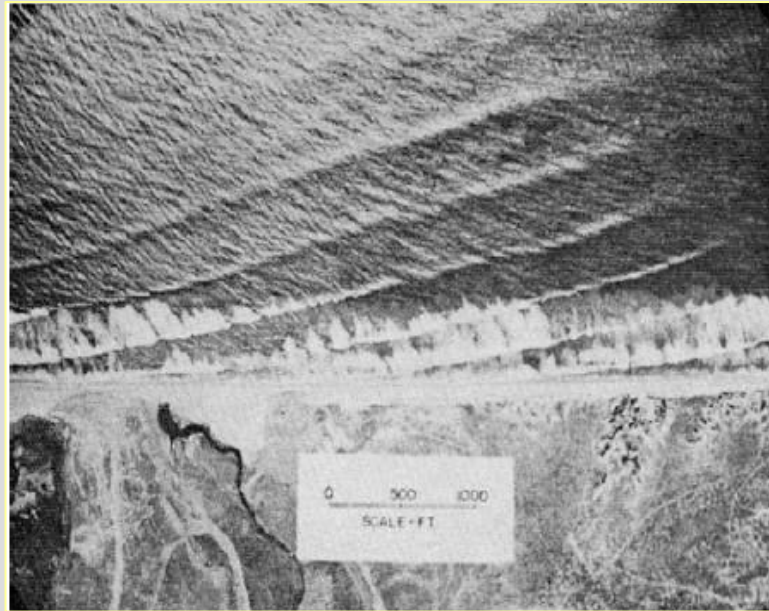
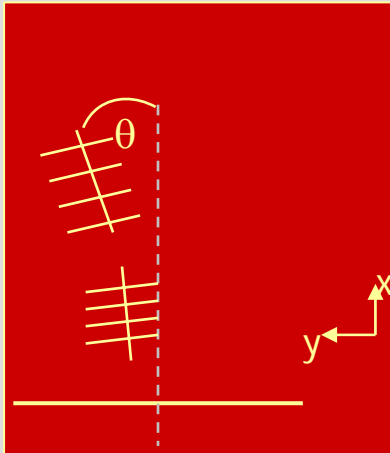
$$\frac{\partial E}{\partial t} + \vec{\nabla} \cdot (\vec{c}_g E) = -Diss$$

σ : wave frequency = constant
 g : gravity acceleration
 $\vec{\kappa}$: wave vector
 k : $\kappa \cos \theta$
 l : $\kappa \sin \theta$

\vec{c}_g : group velocity
 E : energy density
Diss: dissipation
 D : water depth

$$E = \frac{1}{8} \rho g H_{rms}^2$$

Boundary conditions (far offshore): $\sigma + \theta +$ root mean square wave height (H_{rms})



$$\sigma^2 = g\kappa \tanh(\kappa D)$$

$$\frac{\partial \vec{K}}{\partial t} + \vec{\nabla} \sigma = 0$$

$$\frac{\partial k}{\partial y} = \frac{\partial l}{\partial x}$$

$$\frac{\partial E}{\partial t} + \vec{\nabla} \cdot (\vec{c}_g E) = -Diss$$

$$E = \frac{1}{8} \rho g H_{rms}^2$$



wave orbital velocity

$$U_w = \frac{\sigma H_{rms}}{2 \sinh(\kappa D)}$$

used to compute

- bottom stress experienced by current
- sediment transport

Currents

Depth-averaged shallow water equations

$$\frac{\partial \vec{v}}{\partial t} + (\vec{v} \cdot \vec{\nabla}) \vec{v} + f \vec{e}_z \times \vec{v} = -g \vec{\nabla} z_s + \frac{\vec{\tau}_s}{\rho D} - \frac{r u_w \vec{v}}{\rho D}$$

acceleration

advection

Coriolis

gravitation

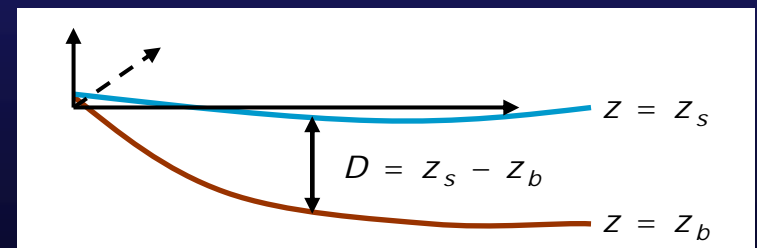
wind
stress

bed shear
stress

- × Only storm conditions considered -> linearized bed shear stress
- × Bottom friction parameter depends on wave orbital velocity
- × Current is driven by (prescribed) wind stress (tides: not important)

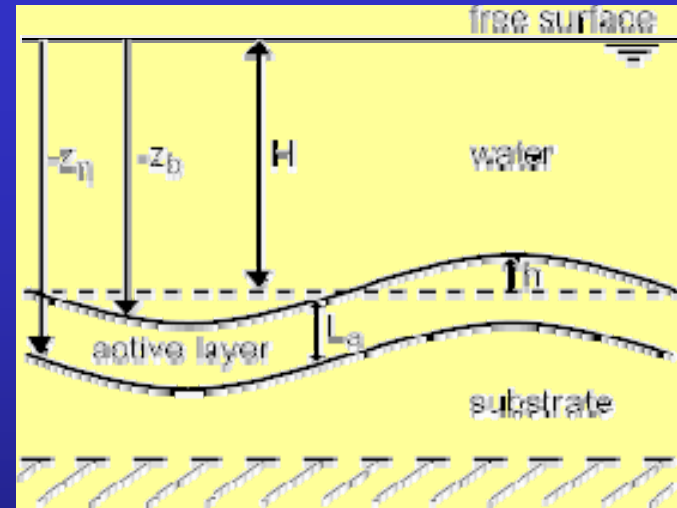
Mass conservation equation

$$\frac{\partial D}{\partial t} + \vec{\nabla} \cdot (D \vec{v}) = 0$$



Sediment mass balance

1 layer model
(no vertical sorting)



For N size fractions:

$$(1 - p) \left\{ F_i \frac{\partial h}{\partial t} + L_a \frac{\partial F_i}{\partial t} \right\} = - \vec{\nabla} \cdot \langle \vec{q}_i \rangle ,$$

$$\sum_{i=1}^N F_i = 1 .$$



two-size
sand mixture
(sizes d_1 and d_2)

where

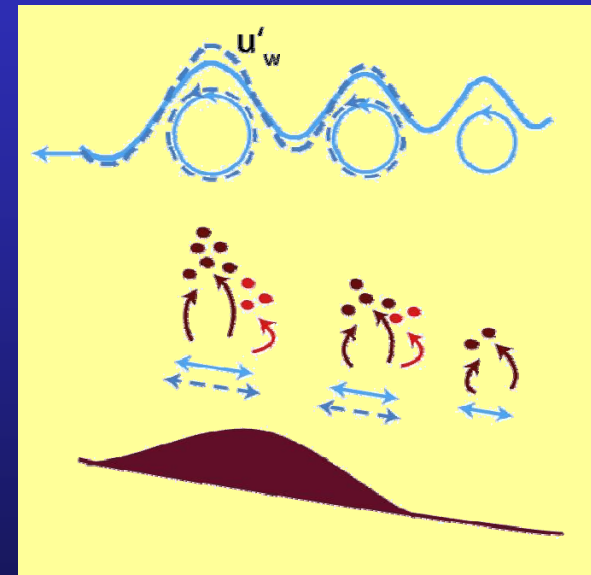
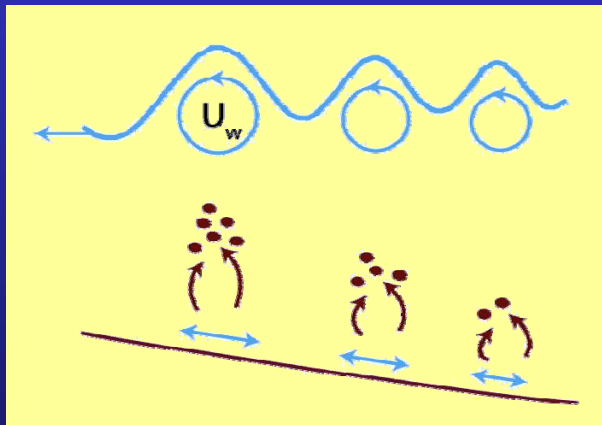
× p : bed porosity

× F_i : fraction of sediment with $\phi_i = -\log_2 d_i$ (size d_i in mm)

Sediment transport and sorting

- Stirring by waves, transport by storm-driven currents
- Effect of local bedslope

stirring of
sediment by
waves



- Only dynamic hiding
(fine grains feel less effective shear stress)
- Formulation hiding functions: Day + Garcia/Parker

Sediment transport and sorting

$$\vec{q}_i = F_i \{ G_{bi} \vec{q}_b + G_{si} \vec{q}_s \} ,$$

$$G_{bi} = \left(\frac{d_i}{d_m} \right)^{c_b} , \quad G_{si} = \lambda_E^5 \left(\frac{d_i}{d_m} \right)^{c_s} , \quad \lambda_E = 1 - c_\sigma \sigma$$

$$\vec{q}_b = Q_b(u_w) \vec{v} - \lambda_b(u_w) \vec{\nabla} z_b$$

$$\vec{q}_s = Q_s(u_w) D \vec{v} - \lambda_s(u_w) \vec{\nabla} z_b$$

advective

bedslope

where

- × F_i : fraction of sediment with $\phi_i = -\log_2 d_i$ (size d_i in mm)
- × G_{bi} : hiding function bedload transport (c_b : coefficient)
- × G_{si} : hiding function suspended load transport (c_s : coefficient)
- × c_σ : coefficient, σ sorting (standard deviation)
- × d_m : mean grain size

Stability analysis

| | Basic state | | Perturbation |
|-----------------|-------------|-----|----------------------------|
| $\mathbf{v} =$ | $(0, V)$ | $+$ | $(u(x, y, t), v(x, y, t))$ |
| $\mathcal{C} =$ | C | $+$ | $c(x, y, t)$ |
| $z_s =$ | ζ | $+$ | $\eta(x, y, t)$ |
| $z_b =$ | $-H$ | $+$ | $h(x, y, t)$ |

Basic state

$$\mathbf{v} = (0, V(x))$$

$$\mathcal{C} = C(x)$$

$$z_s = s_* y + \xi(x)$$

$$z_b = -H(x)$$

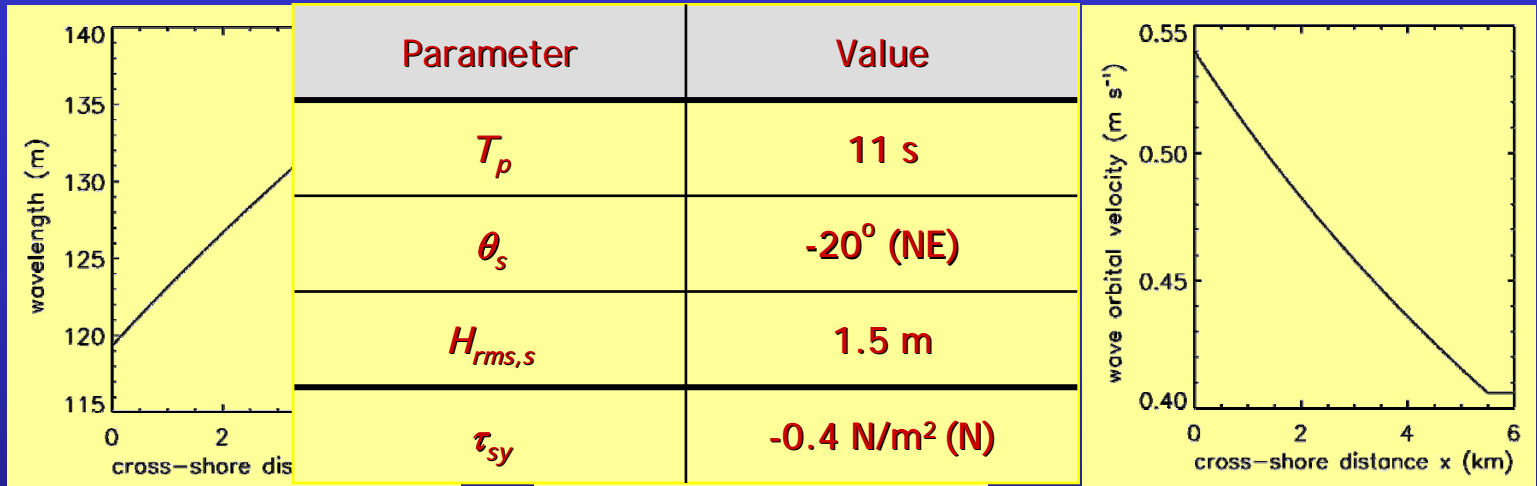
$$fV = g \frac{d\xi}{dx}$$

$$0 = -g s_* + \frac{\tau_{sy} - \tau_{by}}{\rho H}$$

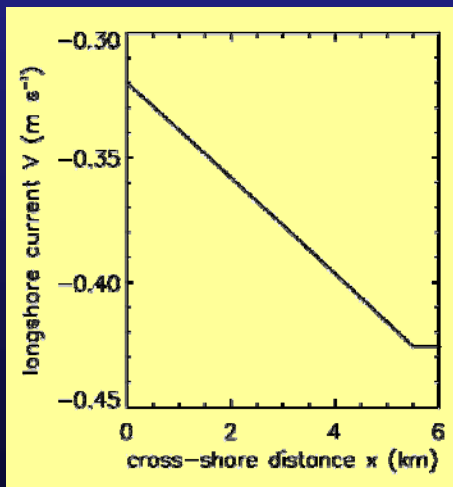
$$0 = \left(\frac{u_w}{\hat{u}} \right)^3 - \frac{C}{\delta H}$$

Basic state

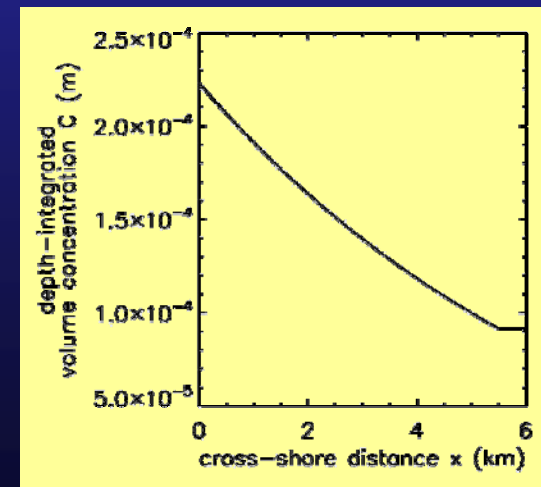
waves



current



sediment concentration



Linear stability

(u, v, η, c, h) small \longrightarrow linearized governing equations

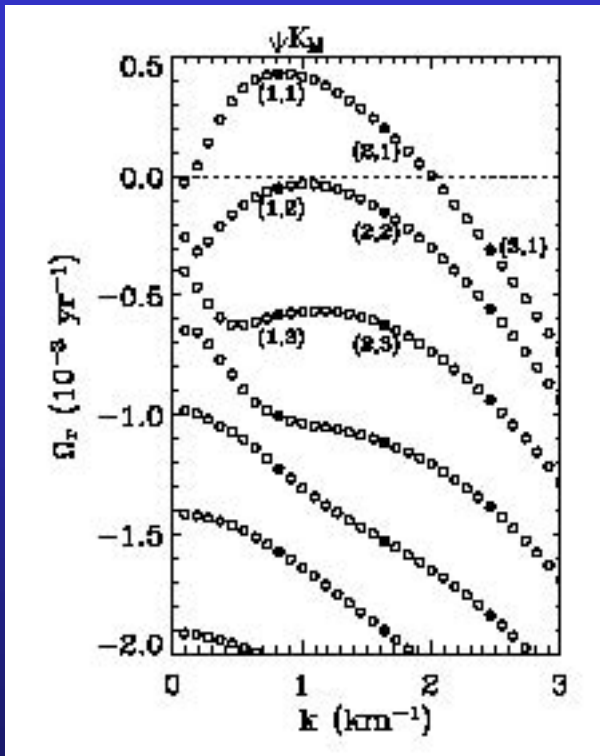
| | Basic state | | Perturbation | |
|---------|---------------|-------------------------|----------------|---------|
| $v =$ | $(0, V(x))$ | $+e^{\omega t} e^{iky}$ | $(u(x), v(x))$ | $+c.c.$ |
| $z_s =$ | $\zeta(x, y)$ | $+e^{\omega t} e^{iky}$ | $\eta(x)$ | $+c.c.$ |
| $C =$ | $C(x)$ | $+e^{\omega t} e^{iky}$ | $c(x)$ | $+c.c.$ |
| $z_b =$ | $-H(x)$ | $+e^{\omega t} e^{iky}$ | $h(x)$ | $+c.c.$ |

\Rightarrow Eigenvalue problem:

- Eigenvalues:
 - Growthrate $\sigma = \text{Re}(\omega)$
 - Migration $c = -\text{Im}(\omega)/k$
- Eigenmodes: (u, v, η, c, h)
 - \longrightarrow patterns emerging from the instability

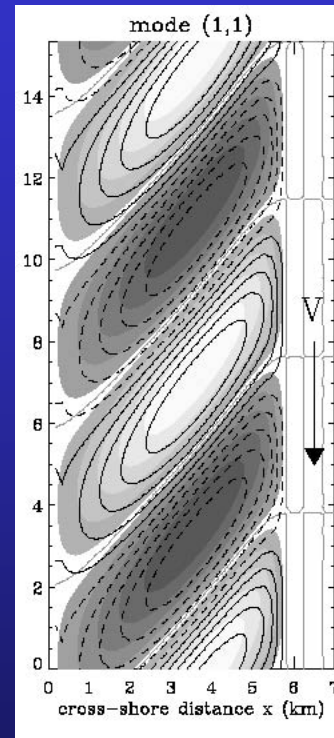
Results of linear stability analysis

parameter values: Long Island inner shelf

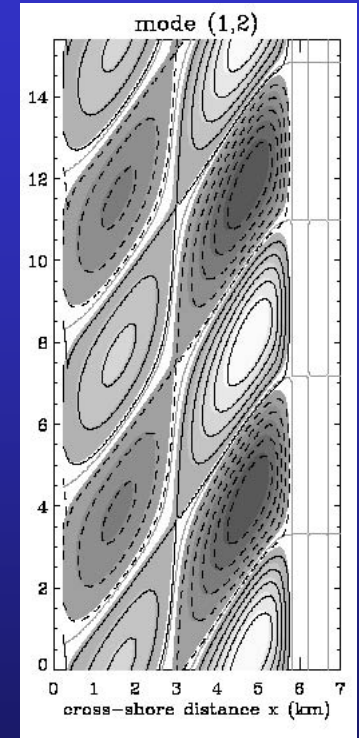


growth rate versus
longshore wavenumber

lengthscale: 7.6 km
timescale: ~ 1000 yr
migration: 2 m/yr



spatial patterns of modes
light colours: crests
solid lines: fine sediment



fine sediment
downstream of crest

Nonlinear model

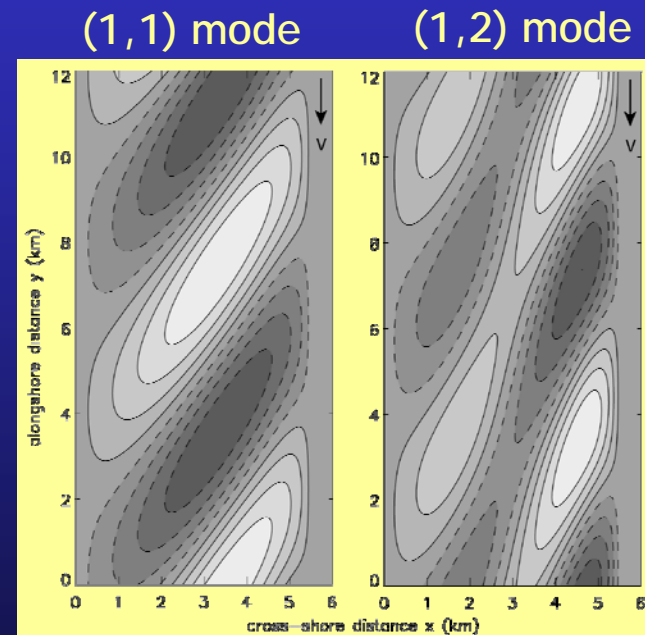
Spectral method: expand perturbations in known eigenmodes
(including the fastest growing mode)

e.g. for bottom

$$h = \sum_{j, n_j} A_{jn_j}(t) h_{jn_j}(x, y)$$

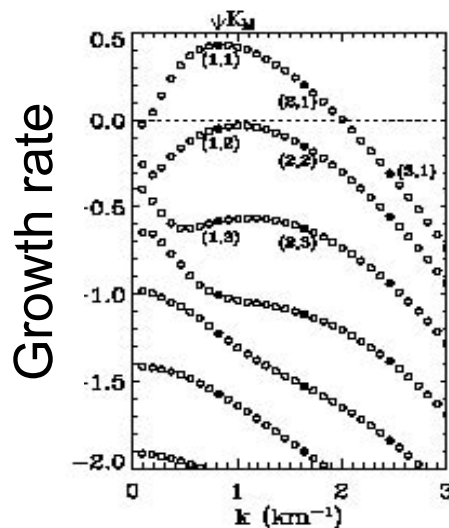


- substitute in equations of motion and project onto adjoint modes
 - differential equations for amplitudes A_{jn_j}
- truncate after a finite number of eigenmodes



Selection of modes

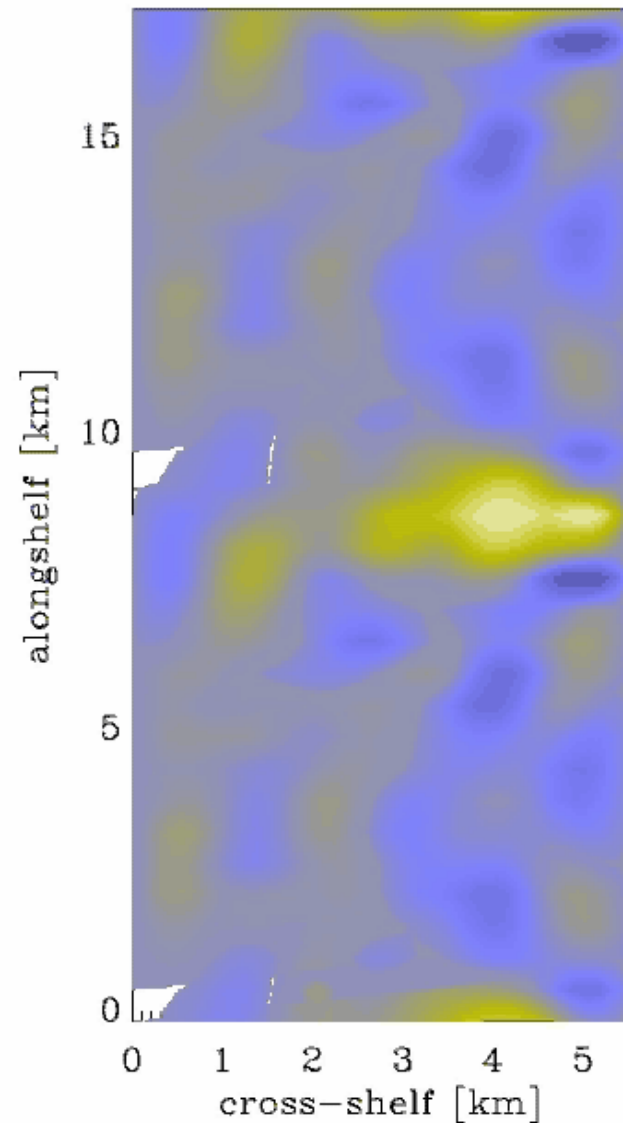
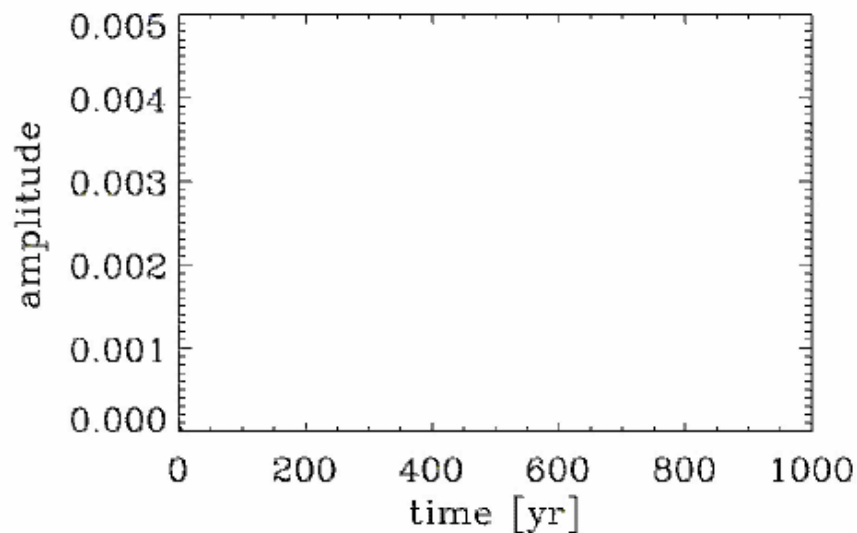
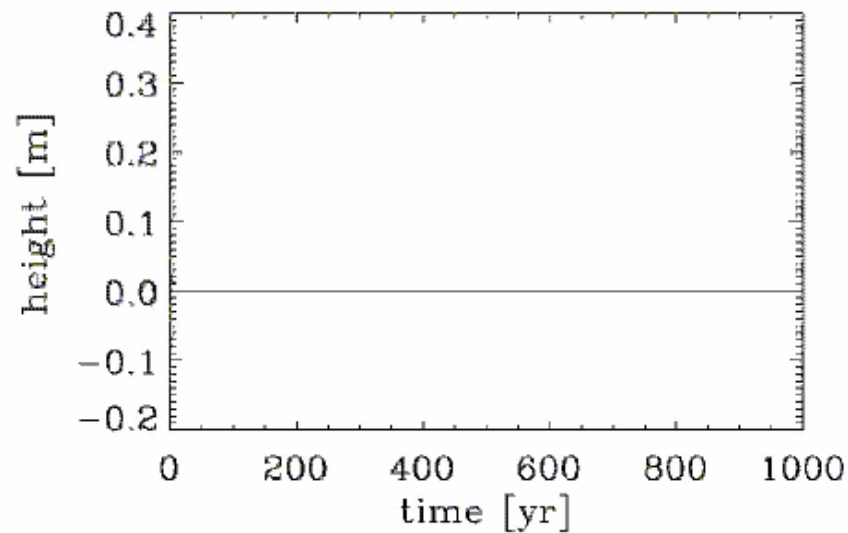
1. Compute eigenmodes of the linearized system
2. Choose domain with longshore length $L=M \times \lambda_{\text{pref}}$ (M integer ≥ 1) with periodic boundary conditions
3. Select eigenmodes of linear system (with wavenumbers k) that fit into this domain:
 - subharmonic modes : $k < k_{\text{pref}}$
 - the basic mode+superharmonics: $k = j k_{\text{pref}}$ ($j=1, \dots, J$)



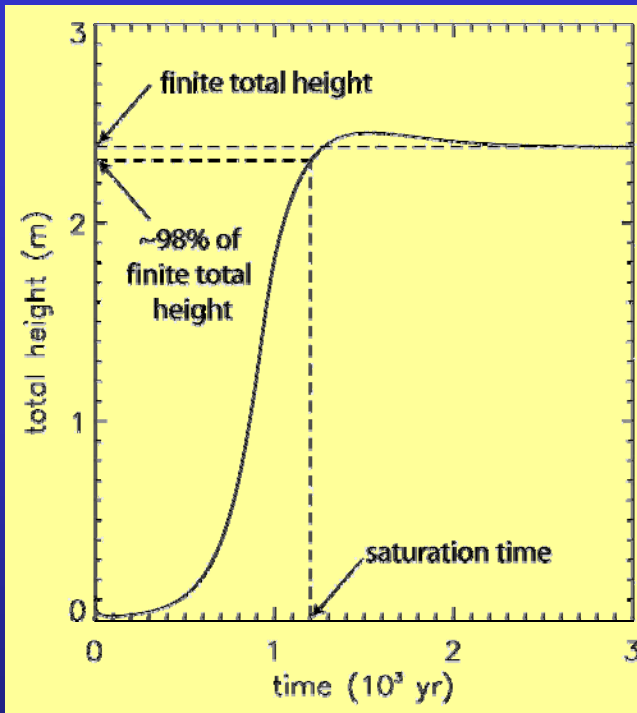
4. For each k : include cross-shore modes with nrs. $1, 2, \dots, N_j$

Animation of default run (no subharmonics)

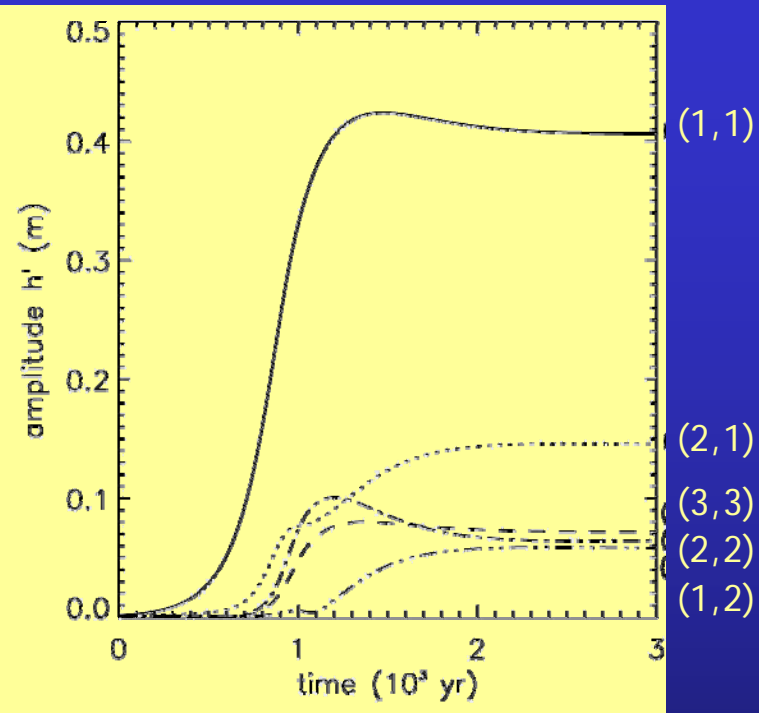
time ~ 5% storms; height/amplitudes x10



$J=64$
 $N_J=10$



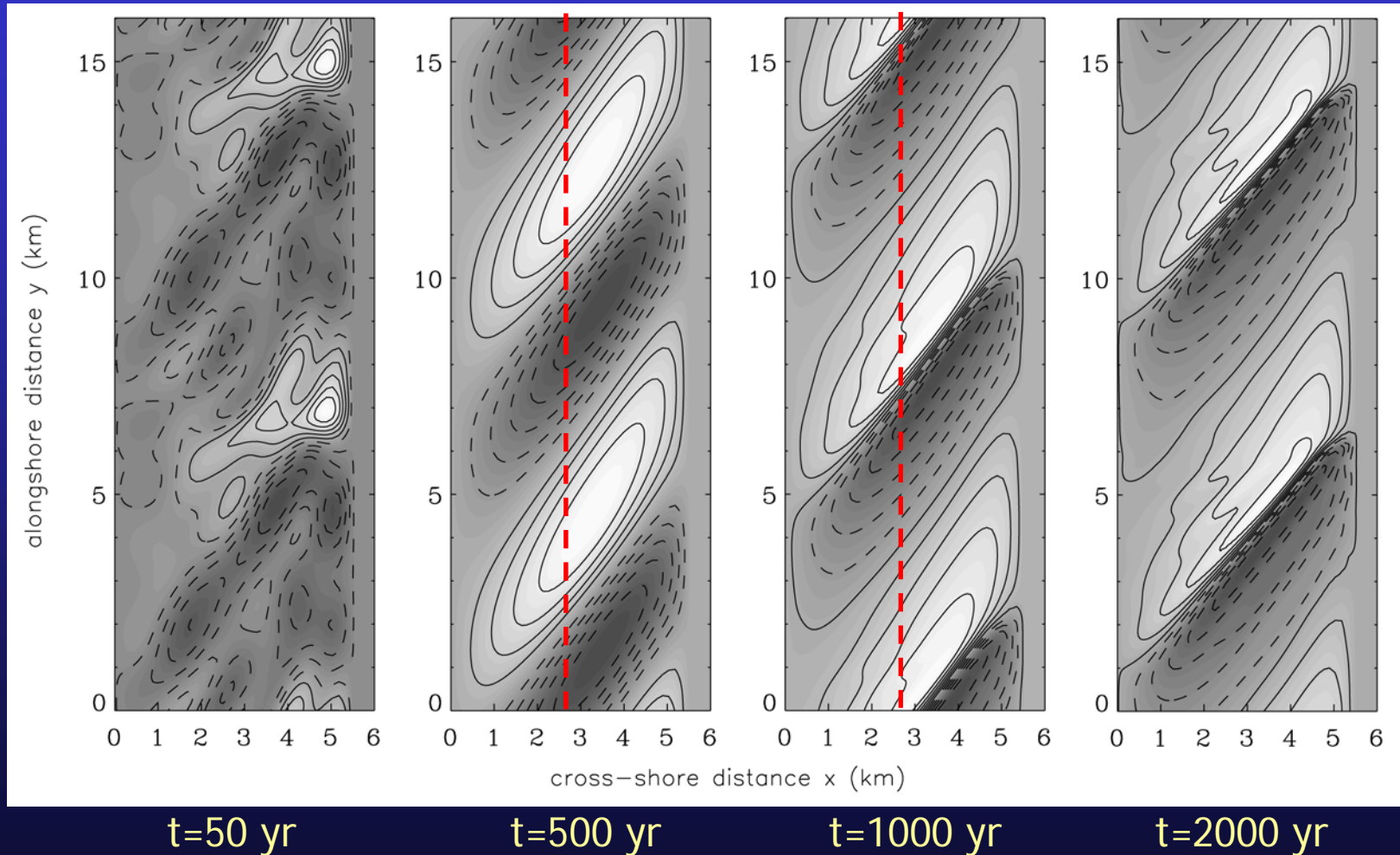
Finite height of the ridges
versus time



Amplitude of five largest bottom
modes versus time

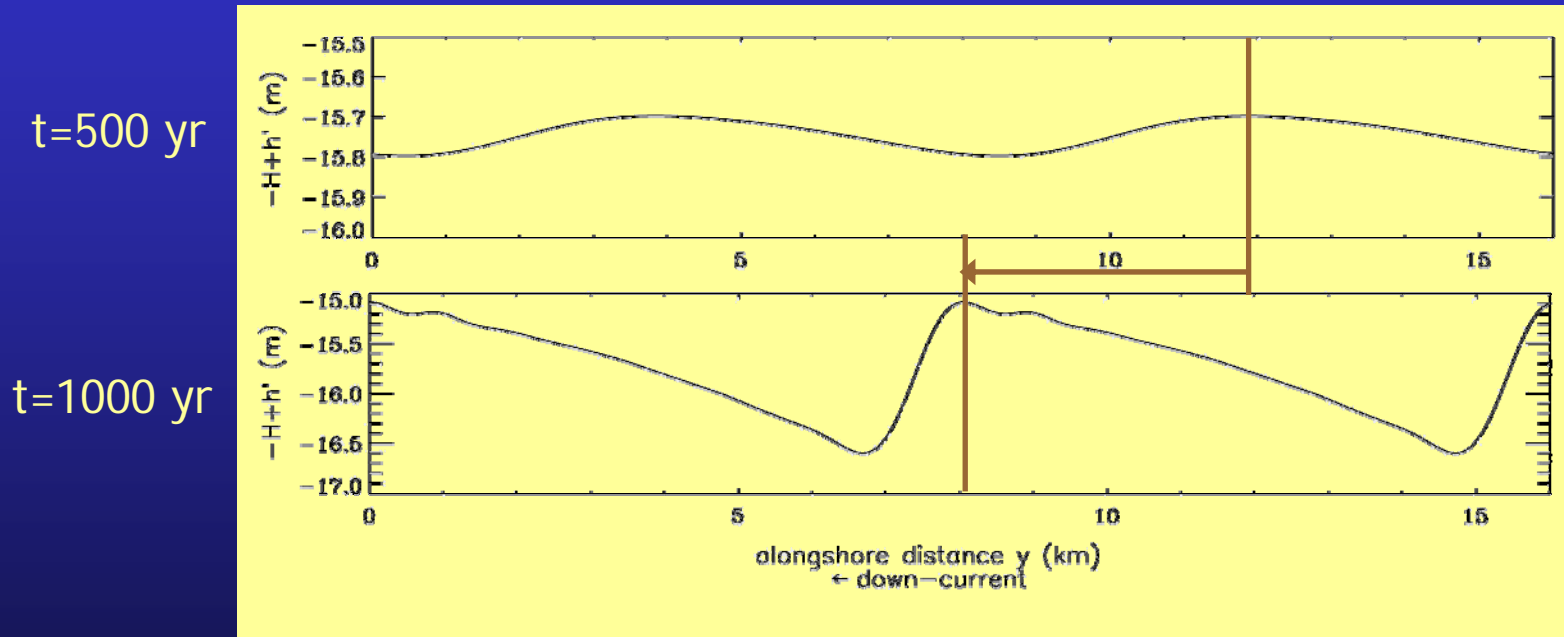
- initial exponential growth, followed by saturation
- initially most preferred mode (1,1) still dominant in saturated state
- model yields problems if transverse bottom slope larger than 60% of the observed value

Bottom patterns during evolution



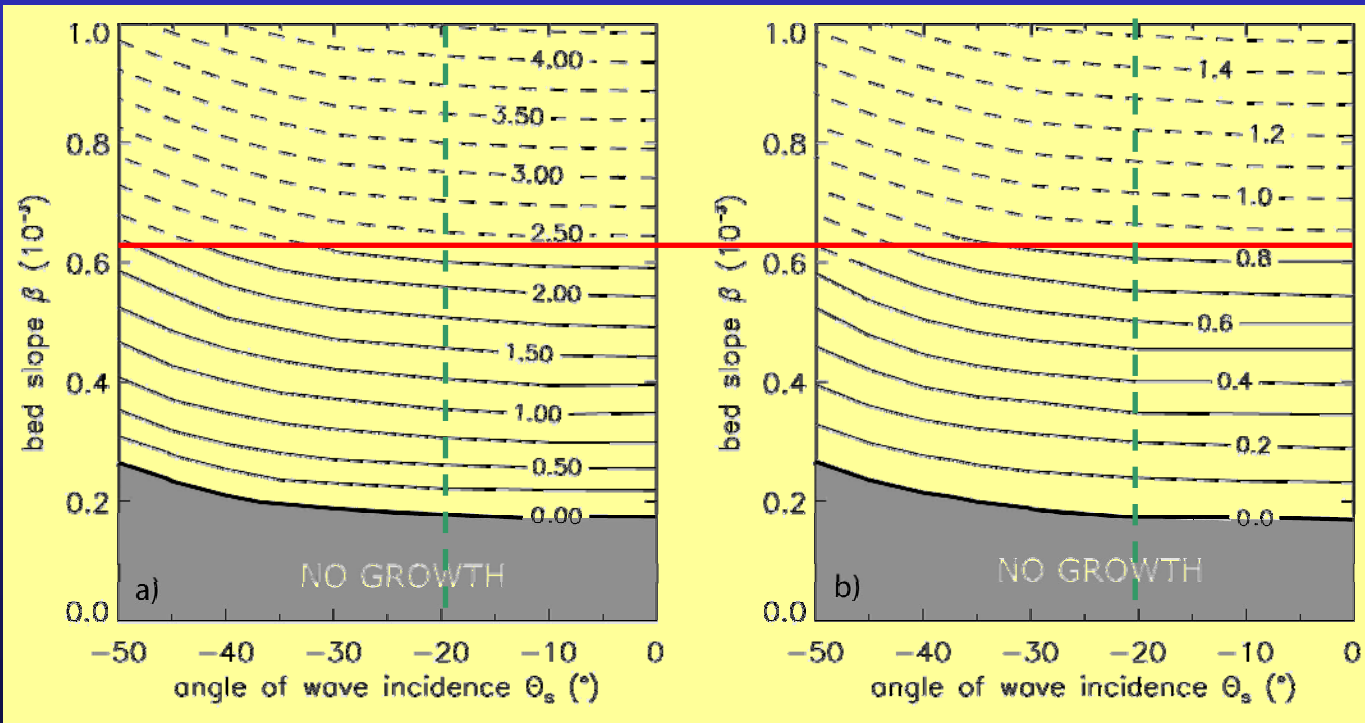
→ bedforms become asymmetric (steep fronts)

Longshore bottom profiles



- steepening of bedforms
- down-current migration of ridges
- constant alongshore spacing ~ 8 km

Sensitivity to offshore angle of wave incidence



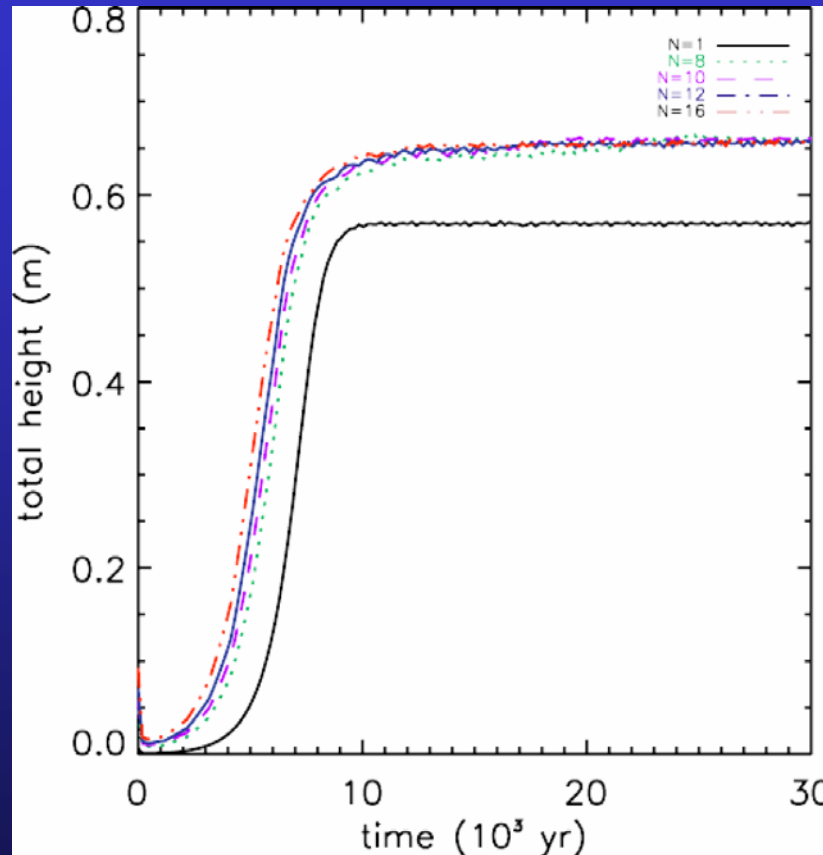
ridge height and saturation time decrease with increasing angle of wave incidence

Lines of equal height of ridges (m) in saturated state

Lines of equal saturation time ($\times 10^3$ year)

Sensitivity to nr. of subharmonic modes (N)

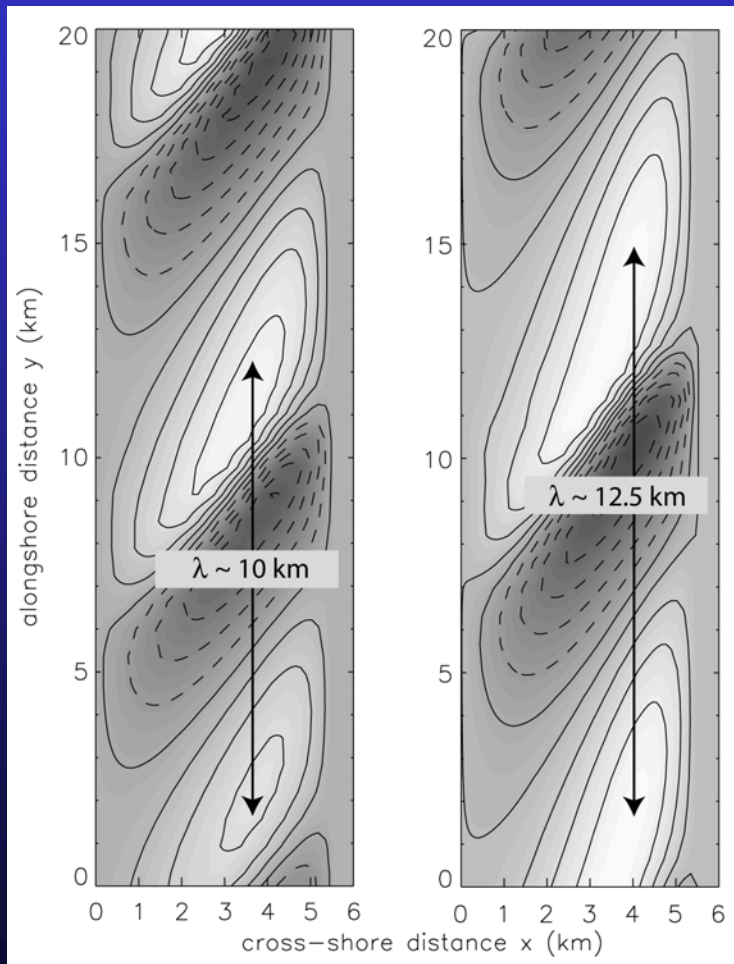
10% of observed bottom slope



- Final height and saturation time only weakly depend on N
 - Bottom patterns at certain time t strongly depend on N
 - If $N > 1$: dominant mode in saturated state has longer wavelength than the initially fastest growing mode
- Remark: bottom slope is 10% of observed value
time scale is ~10x longer, height ~8x smaller

Bottom patterns

10 subharmonics



$t=8000$ yr

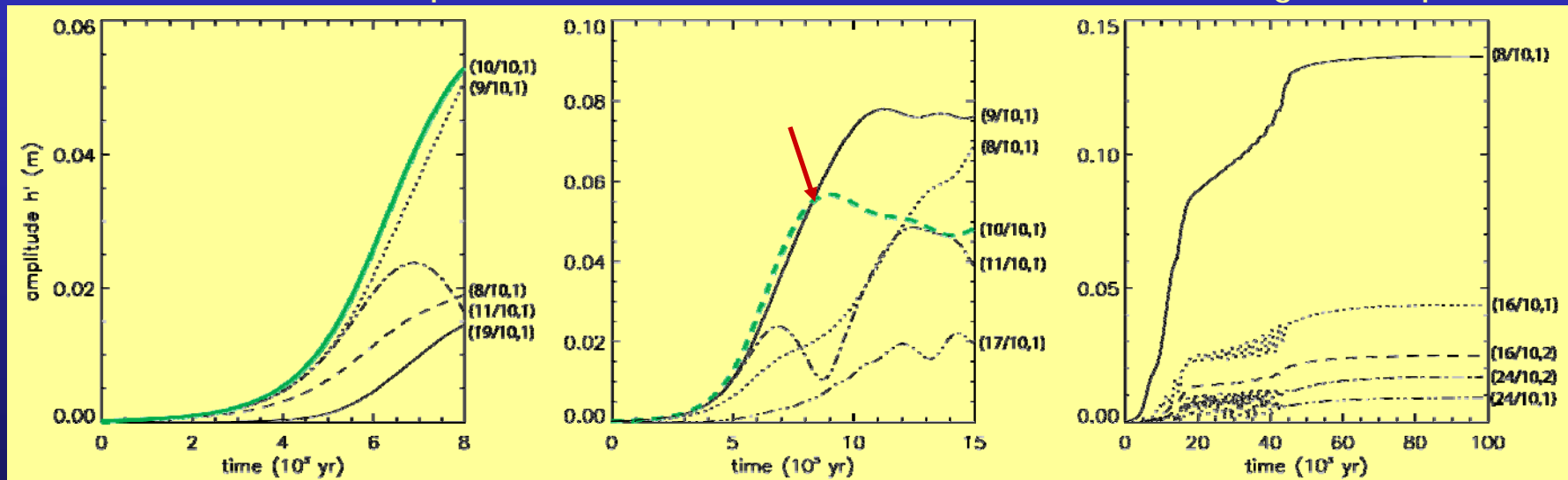
$t=10000$ yr

length scale of the
bedforms becomes larger
during the evolution

Competition between modes

10 subharmonics

Time evolution of amplitude of five bottom modes which have largest amplitude



$t=8000$ yr

$t=15000$ yr

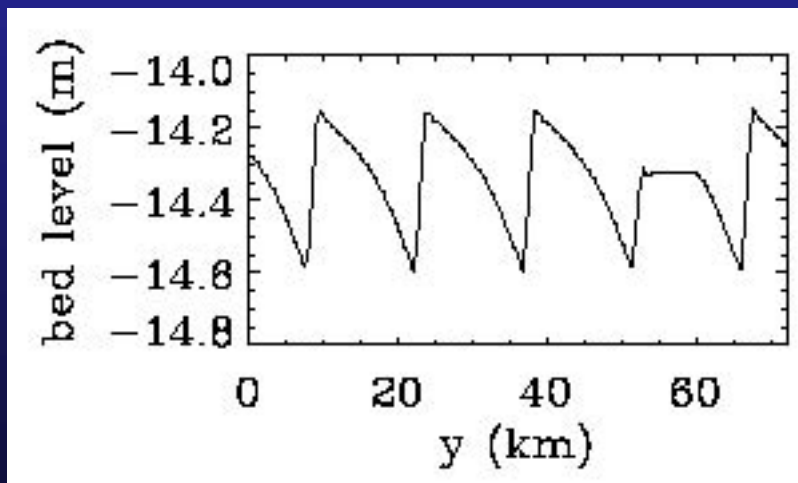
$t=10000$ yr

- First stage: initially most preferred mode dominant
- Second stage: subharmonic modes become dominant
- Third stage: amplitudes of individual modes finally saturate

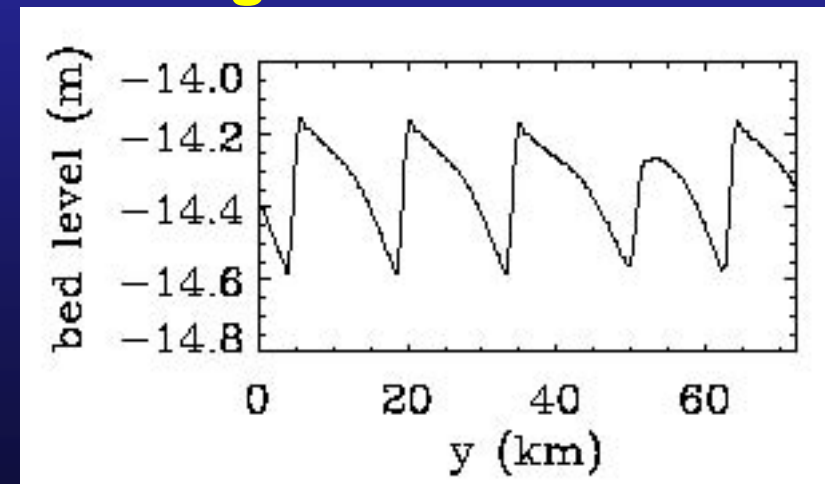
Effect of large-scale interventions on sfcrr and stability of the coastal zone

- Start from a fully developed bottom pattern
- Model an intervention and analyse the subsequent response.
- Type of interventions:
 - extract sand from the inner shelf;
 - dump sand on the inner shelf;
 - construct a navigation channel.

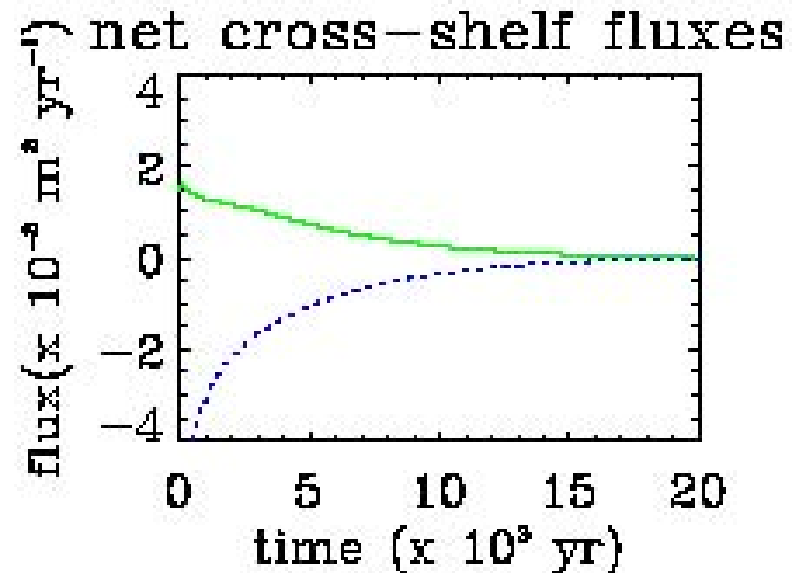
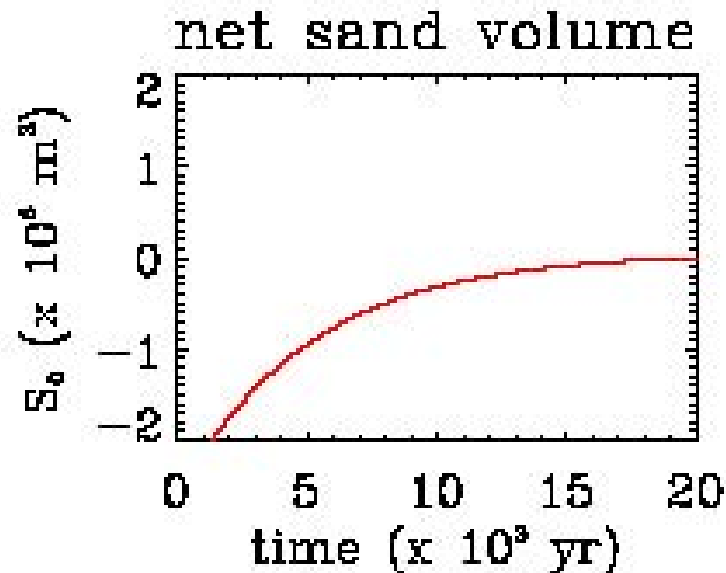
Example: extract sand from a ridge



transect at $x=3\text{km}$, $t=0$



ibid, after 1000 yr



green: beach->shelf
blue: inner->outer shelf

- sand volume inner shelf restores
(timescale $\sim 1000 \text{ yr}$)
- significant cross-shelf fluxes
- negative implications for the beach

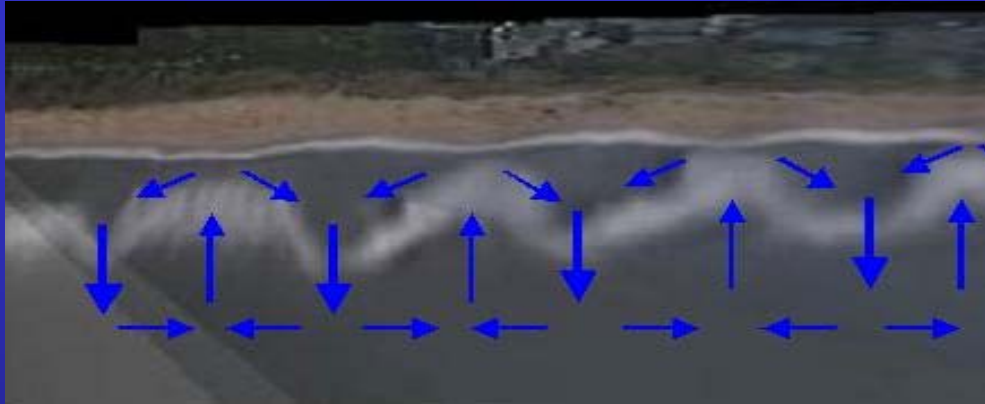
Conclusions (topic A: sfcf)

1. Sfcf can form due to self-organization: transverse slope mechanism
2. Growth mainly due to suspended load transport
(depth-dependent stirring by waves, transport by storm-driven flow)
3. Migration of ridges due to bedload sediment transport
4. Sorting of sediment over sfcf can be modeled
5. Nonlinear spectral model-> saturation behavior
subharmonics results in lengthening of patterns
6. Extraction of sand and dredging of navigation channels have
negative implications for the stability of the beach
(its sand volume decreases).

Present work:

- improve formulations for sediment transport
- account for 3D effects

Topic B: alongshore rhythmic bars



**Crescentic bars
and rip channels**



**Shore-oblique
bars**

Explanations for the formation of rhythmic bars:

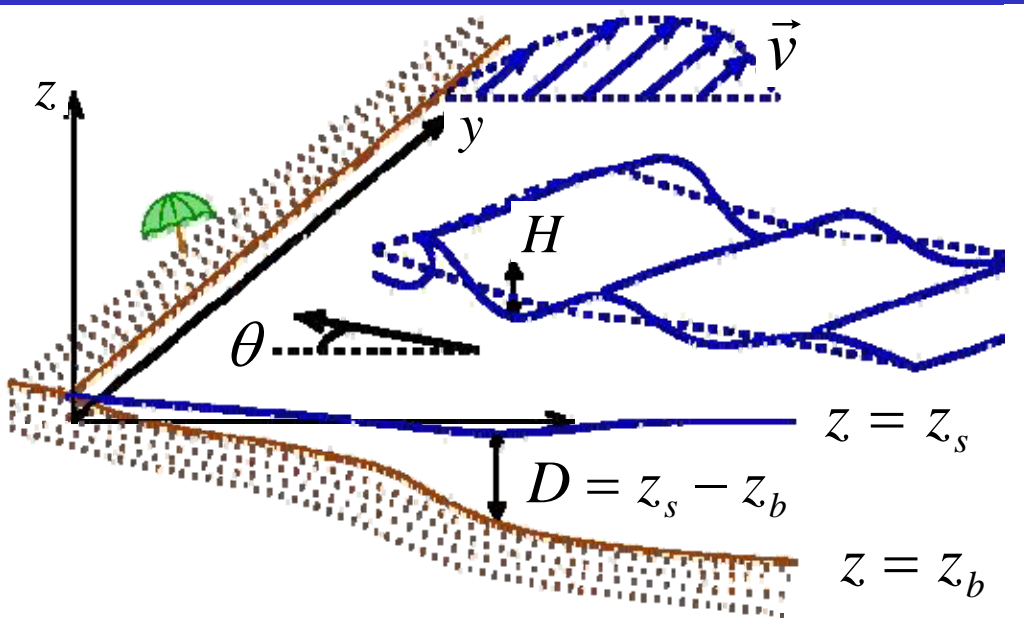
- a) They are forced by infragravity edge waves (Bowen, 1971; Holman and Bowen, 1982)

This explanation has some drawbacks:

- It is not clear in general how these edge waves are generated (with the necessary phase-locking)
- The possible feedback from the developing morphology into the flow is disregarded

- b) They emerge by self-organization of the coupling between flow and morphology (Hino, 1974; Falqués, Coco & Huntley, 2000;)
Essentially, a positive feedback occurs between certain topographic perturbations and the associated perturbations on the waves and currents.

A mechanism for formation of rhythmic topography and rip currents in the nearshore zone



H : wave height

θ : angle of wave incidence

\vec{v} \rightarrow depth-averaged current

$D = z_s - z_b \rightarrow$ water depth

$z_b \rightarrow$ bed level

Waves approaching the coast break and cause

- mean set-up of water level (~ 1 m)
- longshore currents (~ 1 m/s)

Equations of motion:

mass

$$\frac{\partial D}{\partial t} + \frac{\partial}{\partial x_j} (Dv_j) = 0$$

momentum

$$\frac{\partial v_i}{\partial t} + v_j \frac{\partial v_i}{\partial x_j} = -g \frac{\partial z_s}{\partial x_i} - \frac{1}{\rho D} \frac{\partial}{\partial x_j} (S'_{ij} - S''_{ij}) + \frac{\tau_{bi}}{\rho D} \quad , \quad i = 1, 2$$

Depth-averaged equations for currents

Waves affect currents via

- radiation stresses S_{ij}
- turbulent stresses S'_{ij} (mixing depends on wave breaking)
- bed shear stress (components τ_{bi})

=> Add equations for waves (phase-averaged equations)
They govern frequency ω , wave vector and energy density)

=> Add equation for bed level

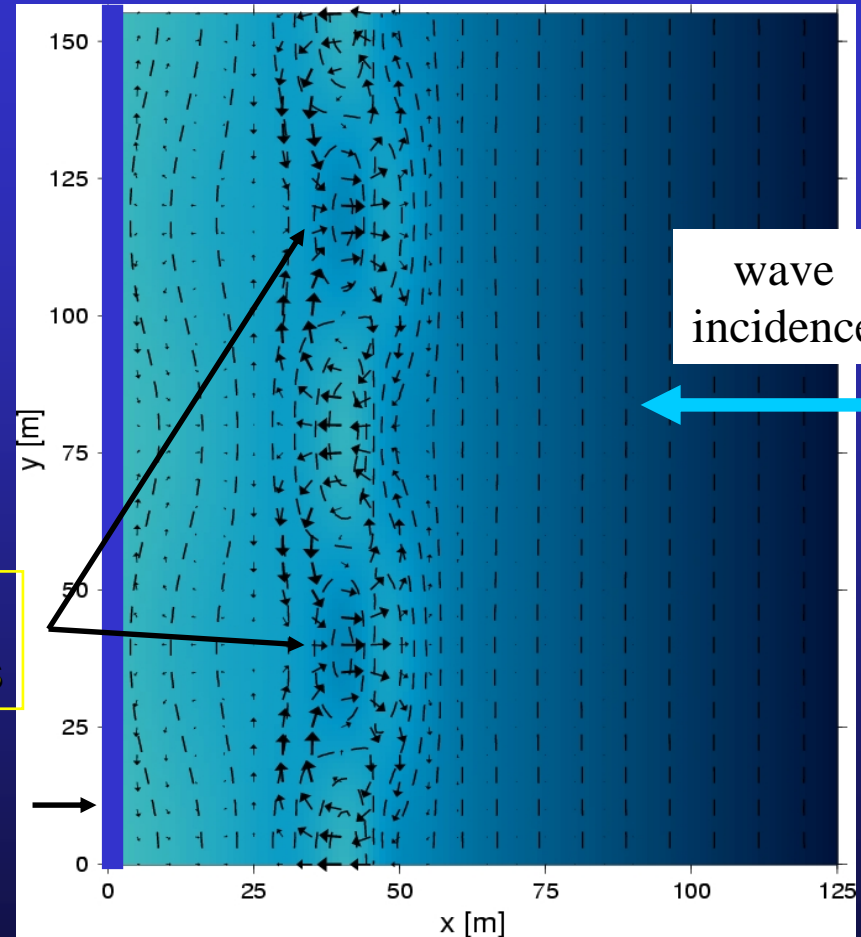
Crescentic bars: linear stability analysis

(Calvete *et al.*, 2005)

- Basic equilibrium topography: linear longshore bar without crescentic pattern
- Can be unstable with respect to growing perturbations in the topography and the flow

Rip currents
and rip channels

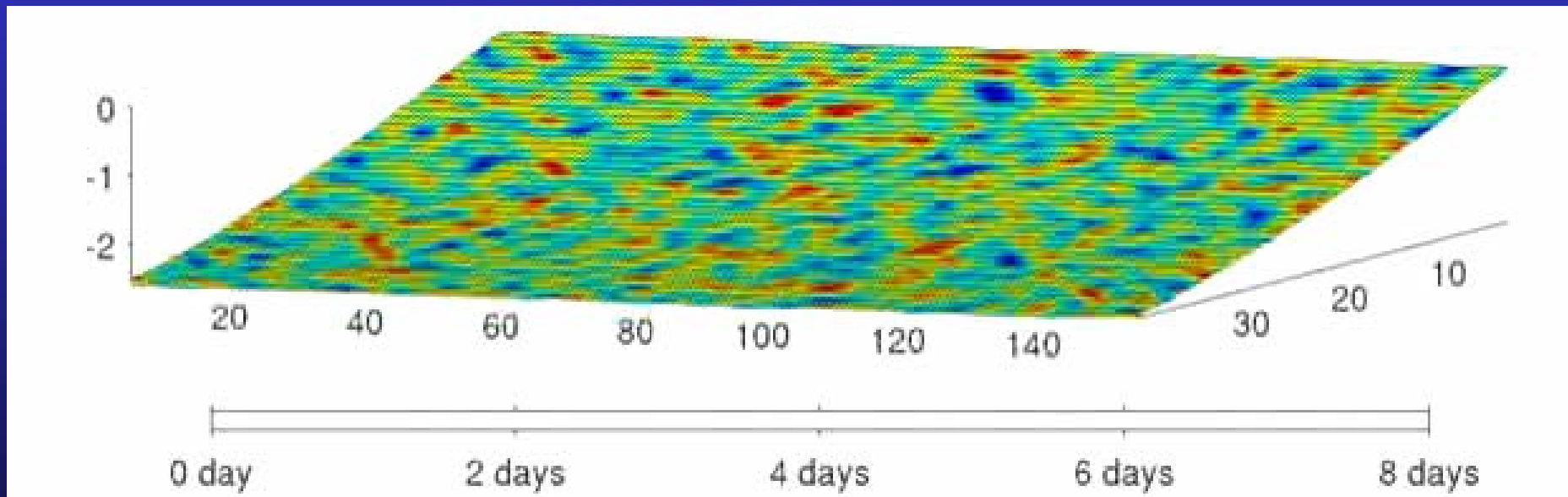
coastline



Instability occurs only for intermediate beach conditions, between fully dissipative and fully reflective

Also when longshore bar is absent bars will emerge

- initial formation (Falqués *et al.*, 2000)**
- long-term evolution using a finite difference model (Caballeria *et al.*, 2002)**



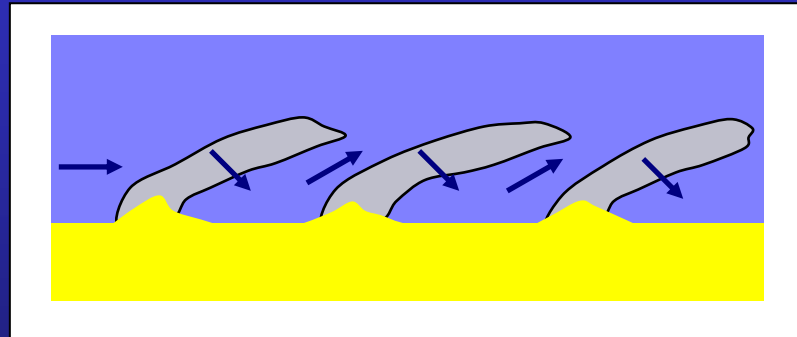
Note the tendency to form larger spacings

Obliquely incident waves

Oblique wave incidence much more complex.

Interaction of:

- 'Bed-surf' effect: Coupling of topography and waves.
- 'Bed-flow' effect: Deflection of the longshore current by the bars.
(similar to sfcrr)

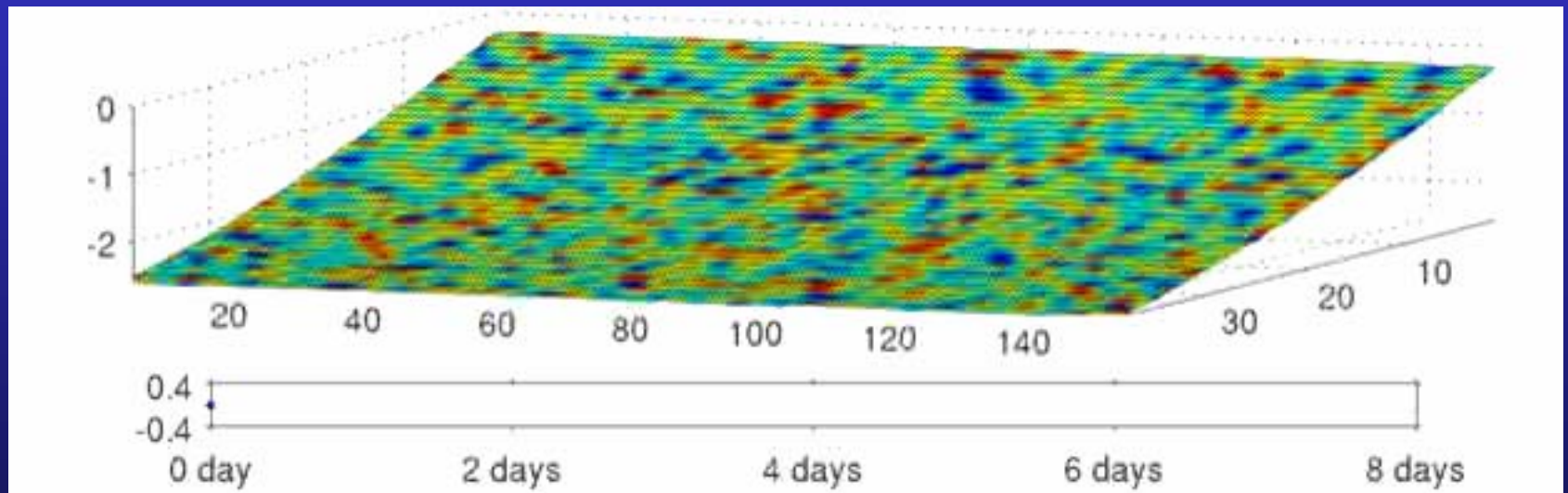


Physical analysis of model reveals that

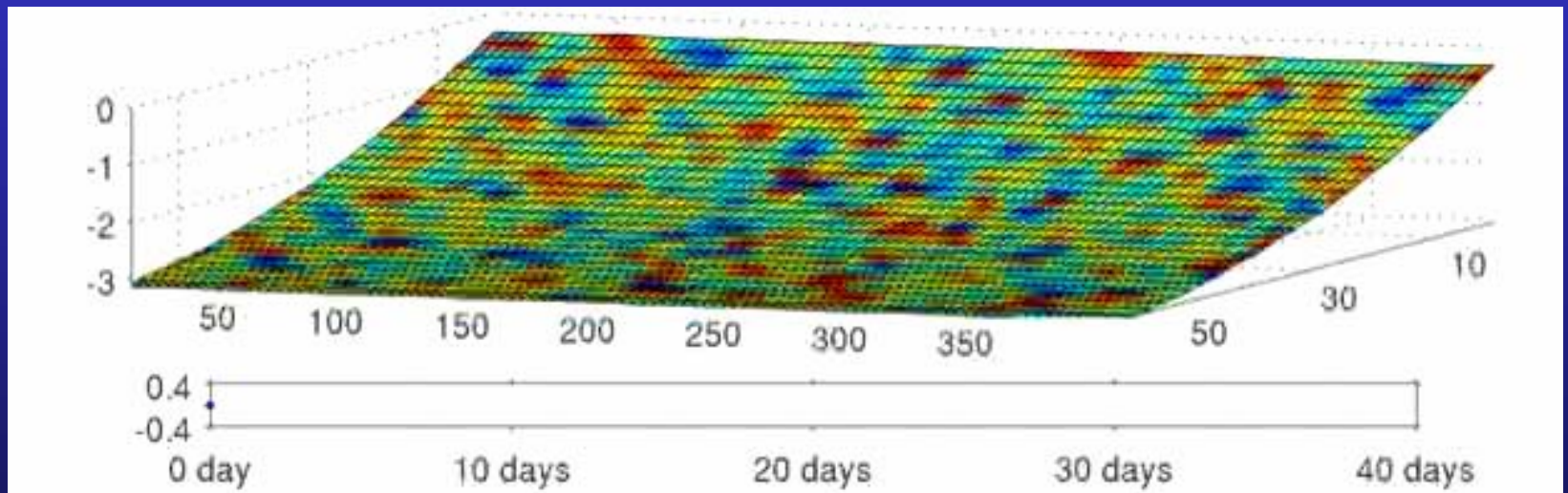
If α/D (\sim depth-mean concentration)

- decreases in offshore direction: upcurrent bars
- increases in offshore direction: downcurrent bars

Finite-amplitude evolution of down-current bars (Garnier *et al.*, 2006)



Finite-amplitude evolution of up-current bars (Garnier et al., 2006)



Conclusions (topic B)

1. The equilibrium beach profile can be unstable to alongshore non uniform perturbations.
2. The instabilities take place for intermediate beach conditions
3. A number of different surf zone rhythmic bar systems can emerge from these instabilities :
 - Crescentic bars
 - Shore oblique / transverse bars
4. The physical process leading to the formation of the bars is a positive feedback between topography and hydrodynamics:
 - 'bed-surf' coupling
 - 'bed-flow' coupling in case of oblique wave incidence

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