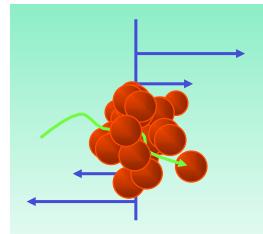


Dispersion Rheology

Dirk van den Ende

Dept. of
Science and Technology
University of Twente



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Outline

Dispersions of non-interacting hard spheres

- Volume fraction dependence
- Brownian particles and Péclet number
- Shear induced diffusion

Soft particle dispersions

Weakly aggregating dispersions

microstructure in relation to

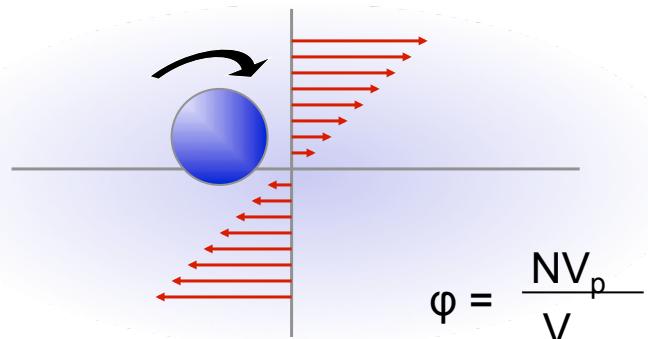
- flowcurve
- linear viscoelasticity

Dispersions out of thermodynamic equilibrium

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Sphere in liquid

- goes with the flow
- has to rotate, additional friction

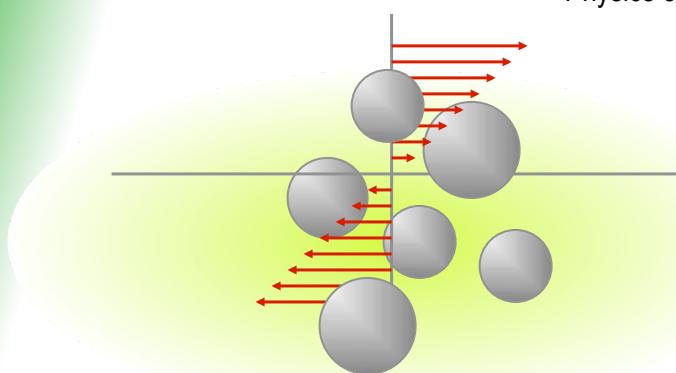


$$\phi = \frac{NV_p}{V}$$

Einstein calculated:

$$\eta = \eta_0 (1 + 2.5\phi)$$

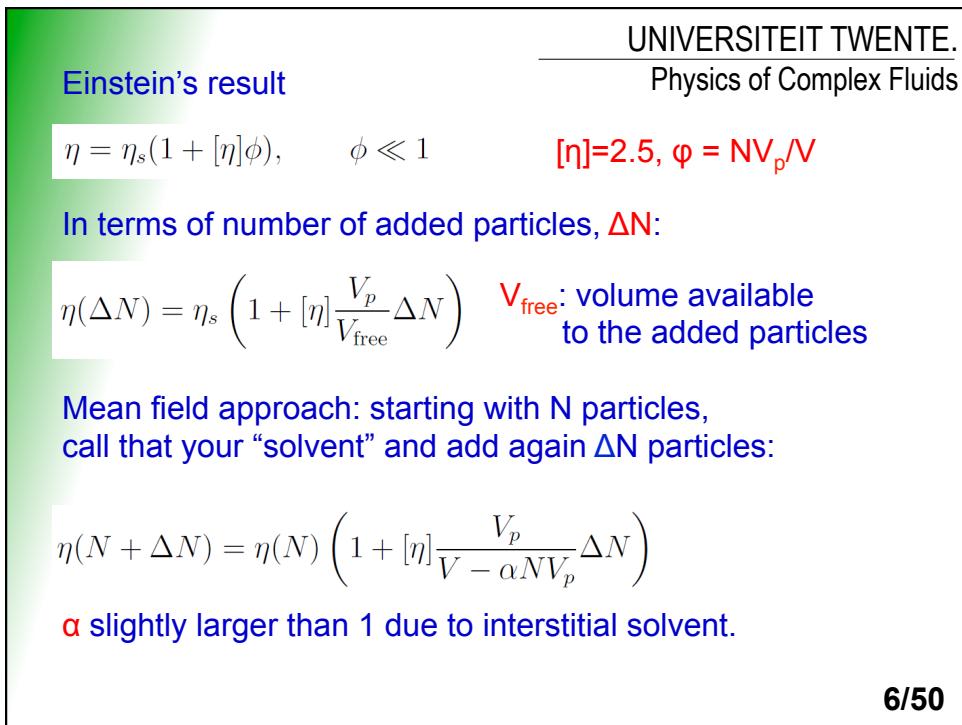
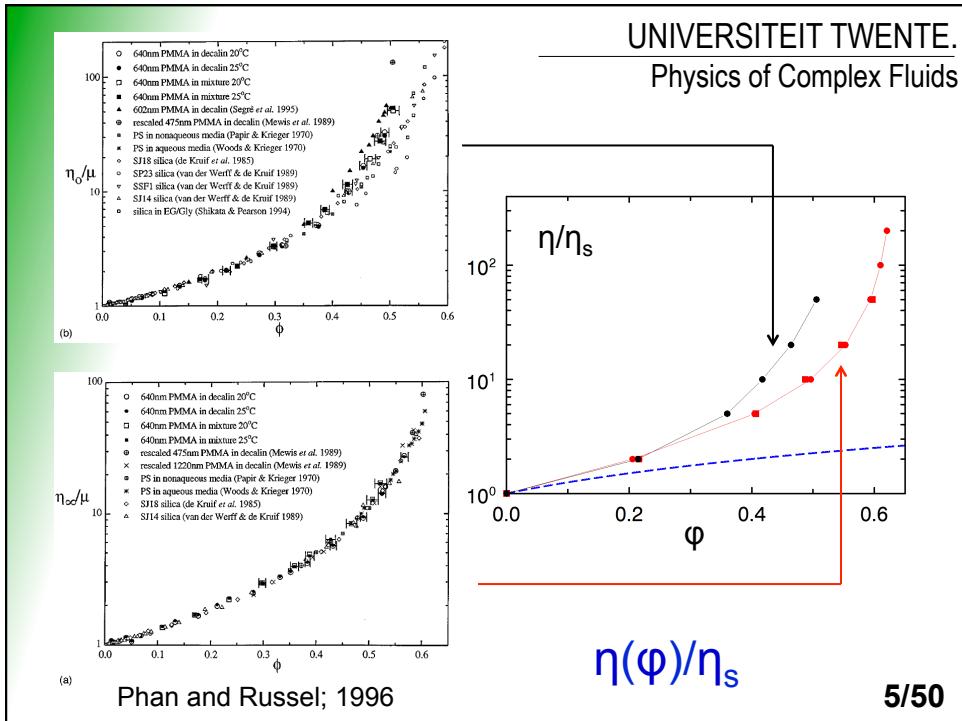
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Dispersions

At higher concentrations

- particles collide with each other
- excluded volume effects

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$$\eta(N + \Delta N) = \eta(N) \left(1 + [\eta] \frac{V_p}{V - \alpha N V_p} \Delta N \right)$$

rewriting this equation

$$\frac{\eta(N + \Delta N) - \eta(N)}{\eta(N)} = [\eta] \frac{V_p}{V - \alpha N V_p} \Delta N = [\eta] \frac{\Delta N V_p / V}{1 - \alpha N V_p / V}$$

or

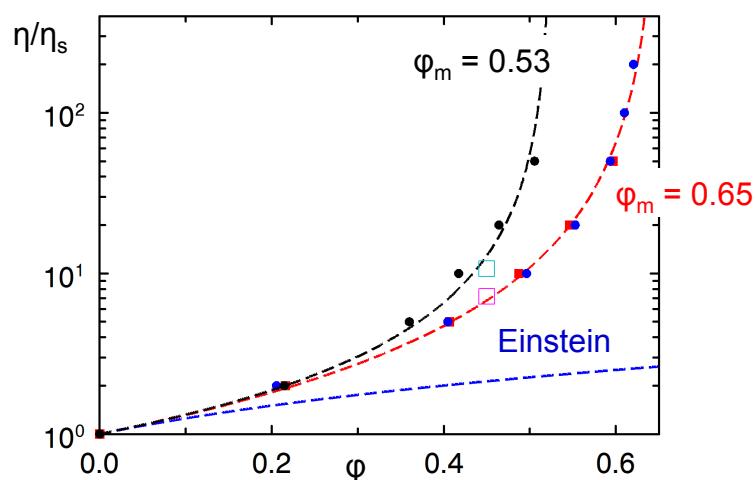
$$\frac{d\eta}{\eta} = [\eta] \frac{d\phi}{1 - \alpha\phi}$$

$$\alpha = 1/\phi_m$$

Krieger Dougerhty equation:

$$\eta = \eta_s (1 - \phi/\phi_m)^{-[\eta]\phi_m}$$

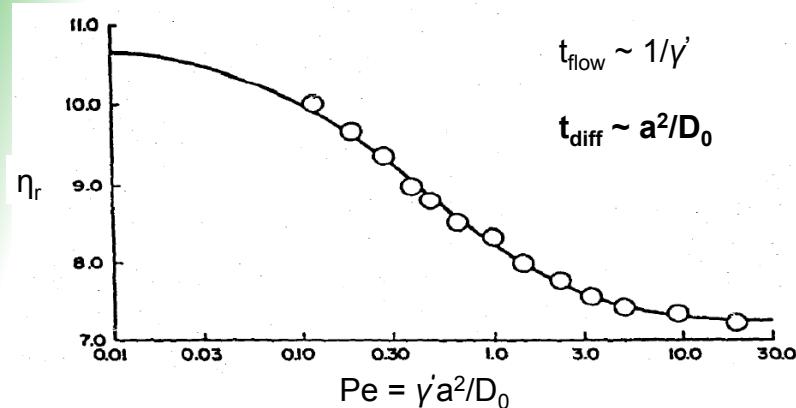
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colloidal particles

competition between diffusion
and convection



polystyrene particles

Krieger, 1972

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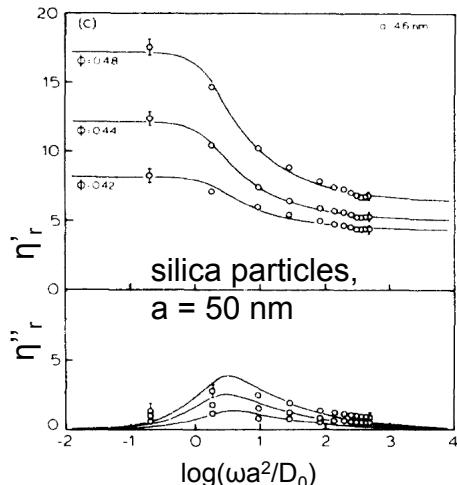
Viscoelastic effects:

HS dispersions show visco-elasticity.

What is the origine of the elasticity?

Entropy and distortion of the pair distribution function $g(r)$

$$\underline{T}^{[str]} = n \int p(\underline{r}) [\underline{r} \underline{F}] d^3 r$$



J. van de Werf et al.; 1989

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Non colloidal particles

shear-induced self-diffusion in simple shear flow

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$$D_{\text{xy}} = a^2 \dot{\gamma} D_{\text{xx}} (\phi)$$

a particle radius

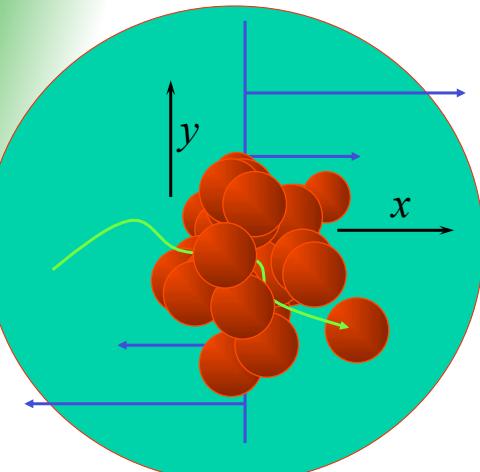
$\dot{\gamma}$ rate of shear

ϕ volume fraction

Tensor character:

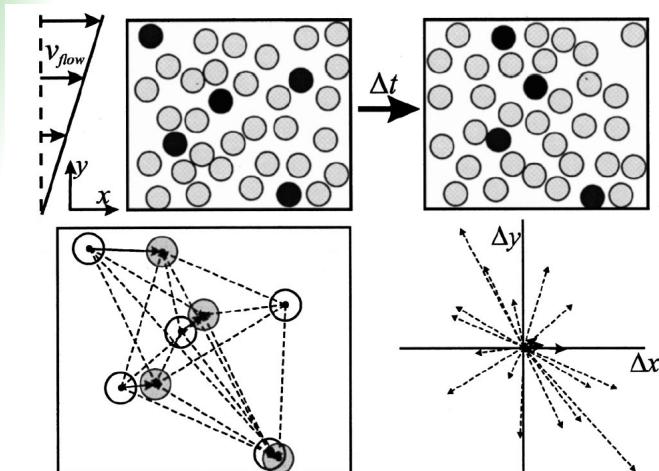
$$\left\{ \begin{array}{ccc} D_{xx} & D_{xy} & 0 \\ D_{yx} & D_{yy} & 0 \\ 0 & 0 & D_{zz} \end{array} \right\}$$

11/50



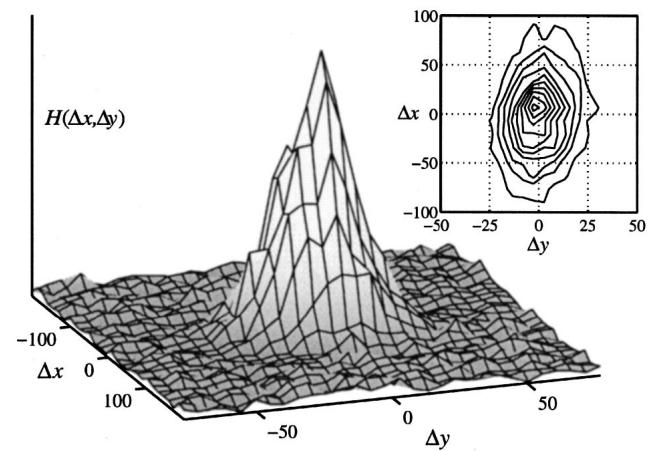
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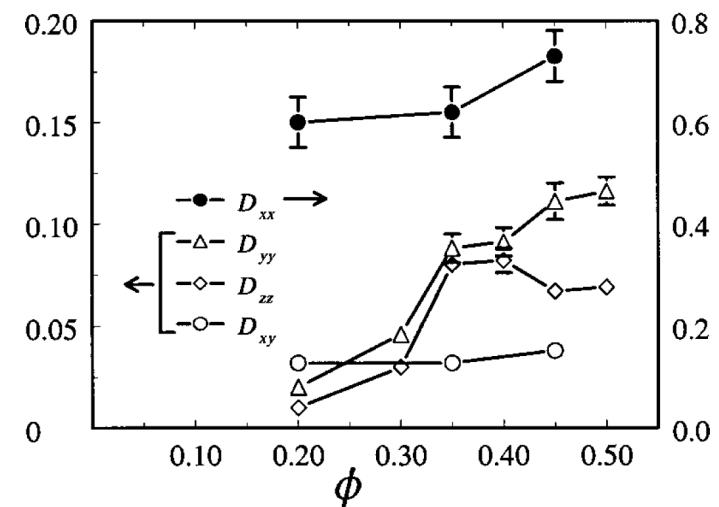


V. Breedveld et al. ; 2002

12/50



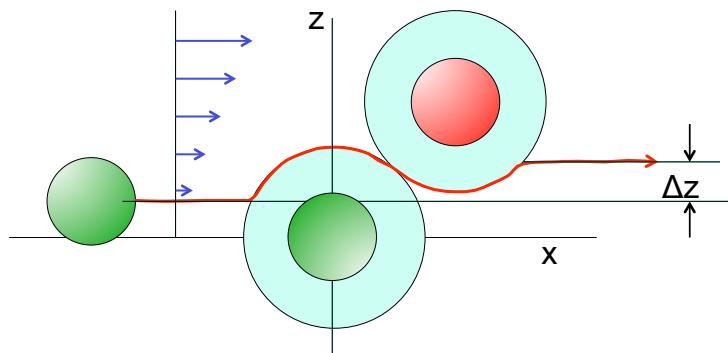
13/50



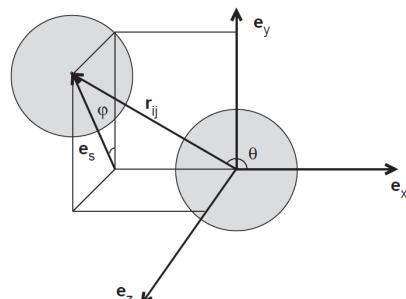
14/50

Simple model

- Particles follow flow lines if not prohibited by excluded volume
- While colliding they role over each other
- Collisions are not completed due to interaction with a third particle



15/50

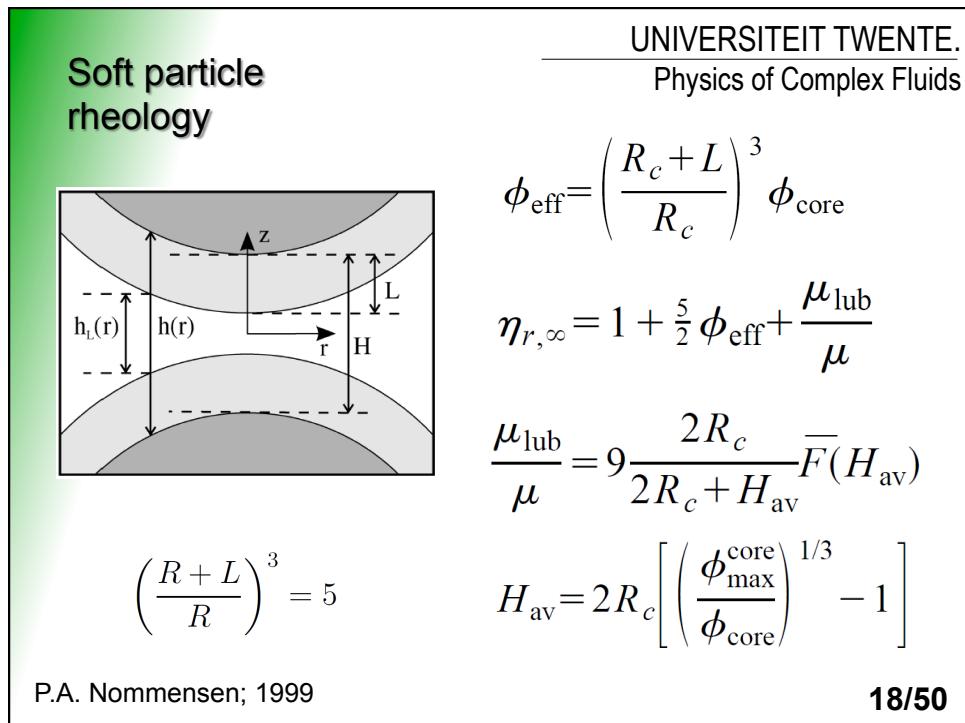
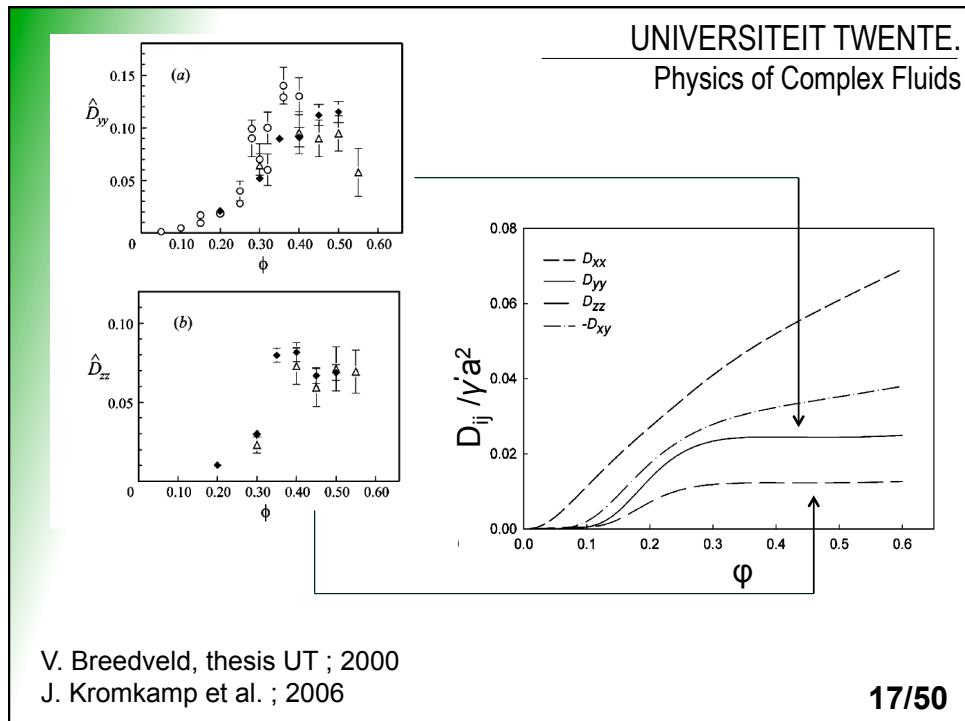


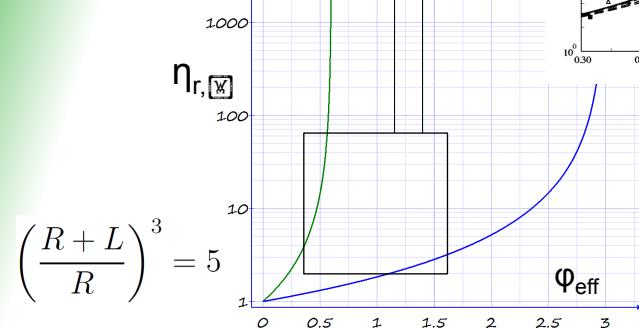
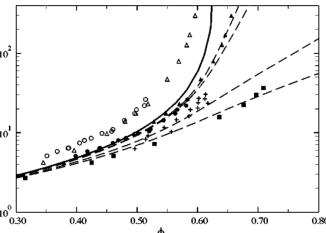
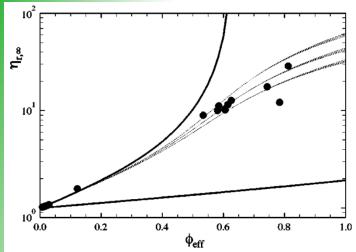
Taking an average collision time $t_c(\phi)$, we calculate the displacement vector $\underline{s}(\theta, \phi)$ per collision.

Diffusion tensor:

$$\underline{D} = \frac{\langle \underline{s} \underline{s} \rangle}{2t_c} = \frac{4\phi\dot{\gamma}}{\pi} \langle \underline{s} \underline{s} \rangle$$

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D'Haene,
thesis Leuven; 1992

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*The mystery
of the missing factor*

3

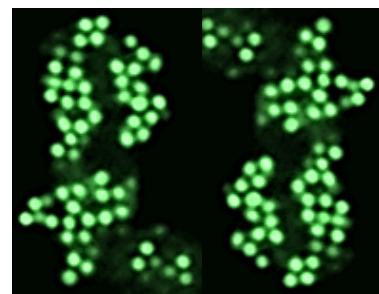
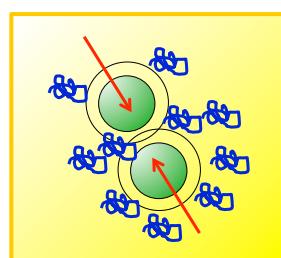
$$\langle \Delta x^2(t) \rangle = \frac{k_B T}{3\pi R} J(t)$$

$$\langle \Delta r^2(t) \rangle = \langle \Delta x^2(t) \rangle + \langle \Delta y^2(t) \rangle + \langle \Delta z^2(t) \rangle = 3 \langle \Delta x^2(t) \rangle$$

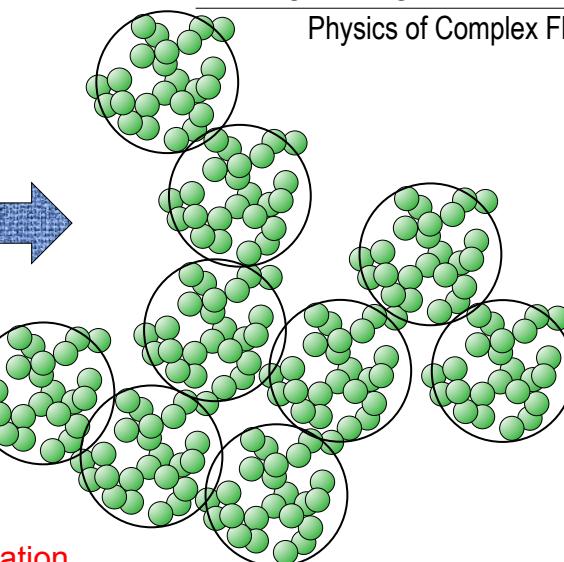
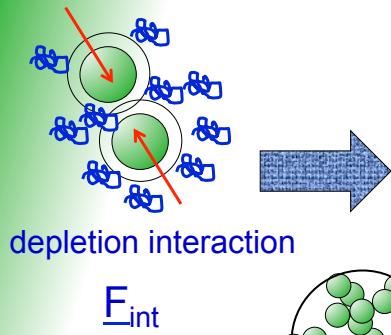
$$\langle \Delta r^2(t) \rangle = 3 \frac{k_B T}{3\pi R} J(t) = \frac{k_B T}{\pi R} J(t)$$

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Weakly aggregating colloidal dispersions



21/50



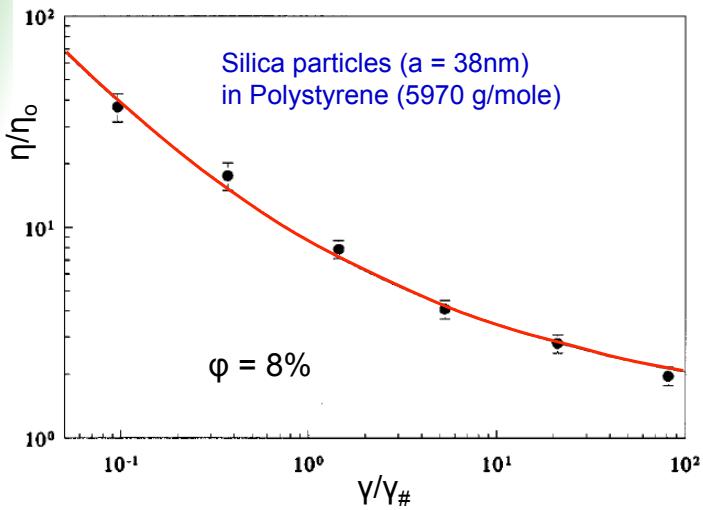
Parameters:

- particle concentration
- polymer concentration and size
- structure of the aggregates

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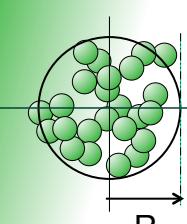
Flow curve

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Wolters et al. 1996

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$$N(R) = N_0 \left(\frac{R}{a} \right)^{d_f} \quad \text{fractal aggregate}$$

$$\text{volume fraction of aggregates: } \phi_a = \frac{\phi_p}{N_0} \left(\frac{R}{a} \right)^{3-d_f}$$

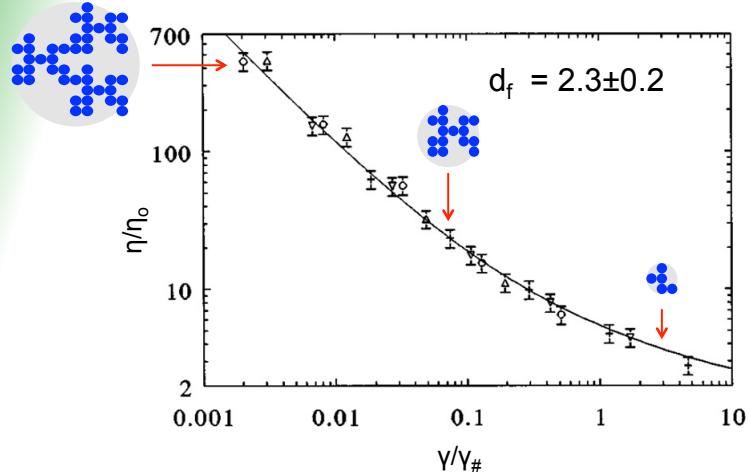
$$F_{\text{int}} \geq F_{\text{hyd}} : \quad F_{\text{int}} = F_{\text{hyd}} = \frac{5}{2} \pi R^2 \eta \dot{\gamma}$$

mean field approximation

viscosity curve:

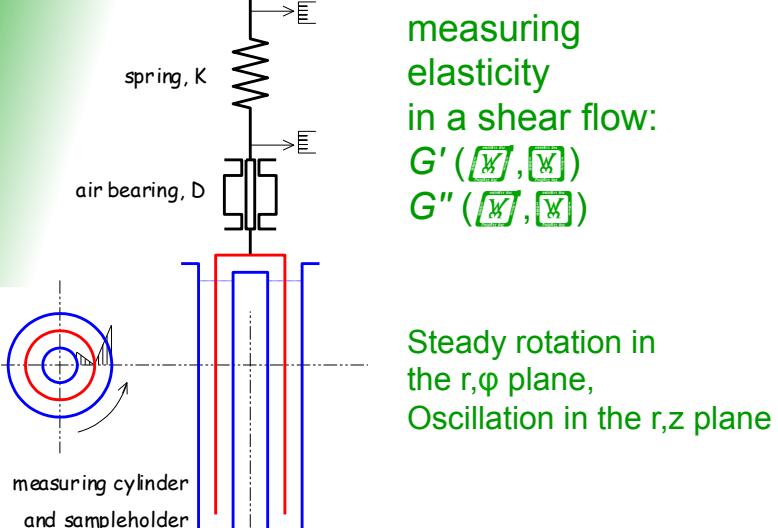
$$\eta = \eta_0 \left(1 + \frac{\phi_p}{\phi_m} \left(\frac{\tau_{\text{int}}}{\eta \dot{\gamma}} \right)^{(3-d_f)/2} \right)^{-2.5\phi_m} \quad \tau_{\text{int}} = \frac{2F_{\text{int}}}{5\pi a^2}$$

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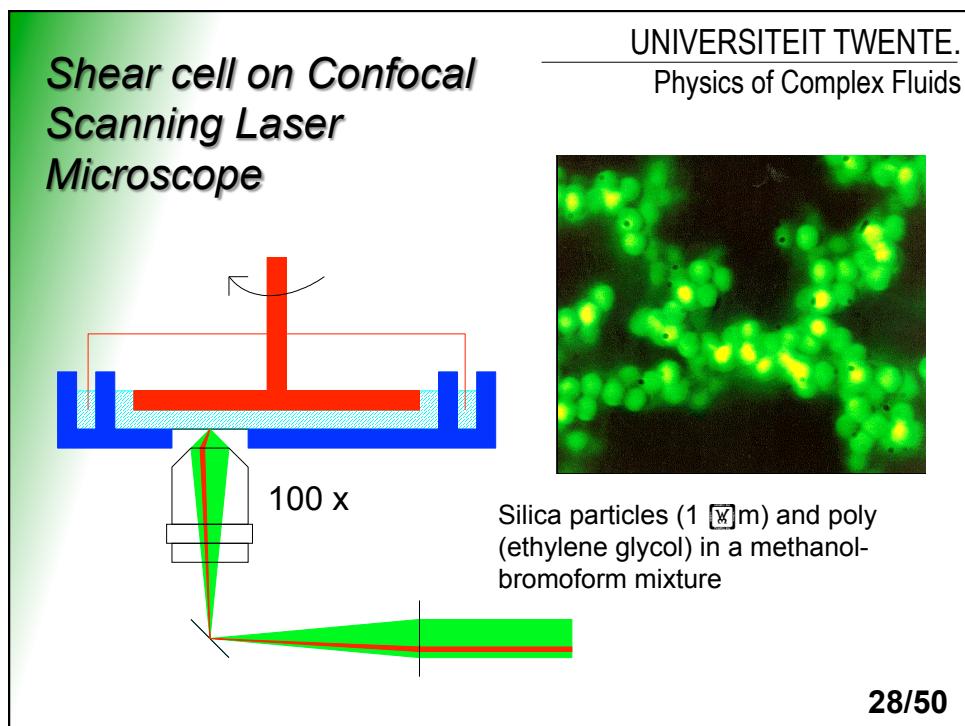
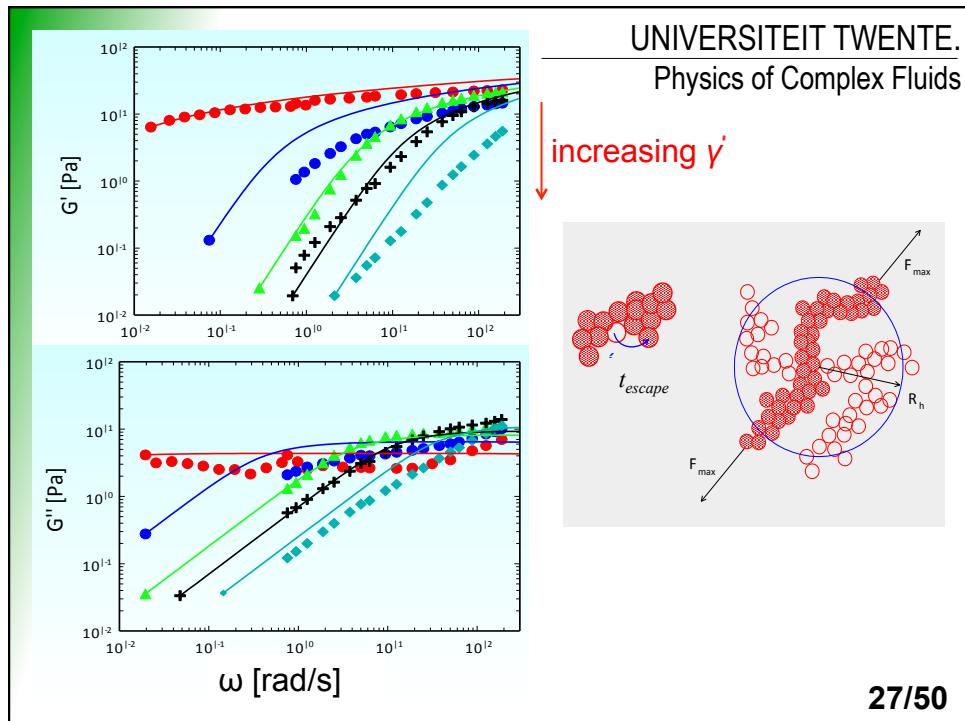
$$\dot{\gamma}_\# = \left(\frac{\phi}{\phi_m} \right)^{2/(3-d_f)} \frac{\tau_{int}}{\eta_0}$$

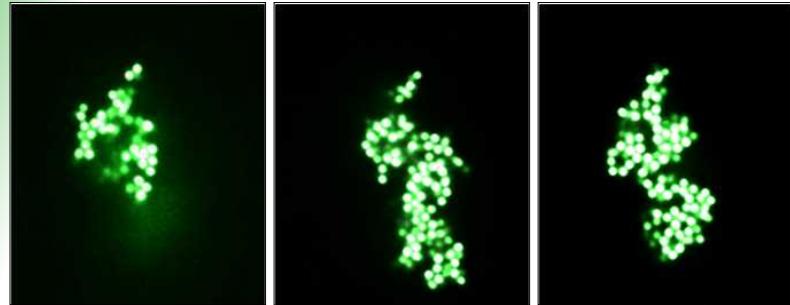
25/50



Zeegers et al. ; 1995

26/50

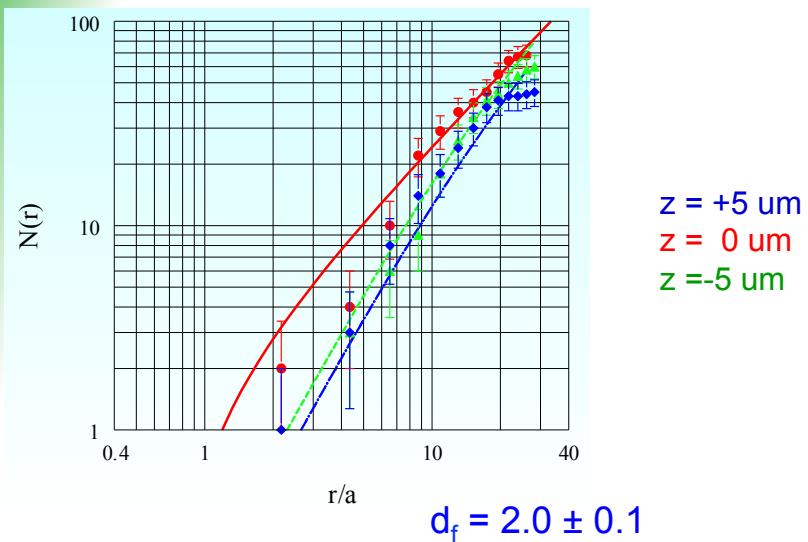




Different cross sections through an aggregate

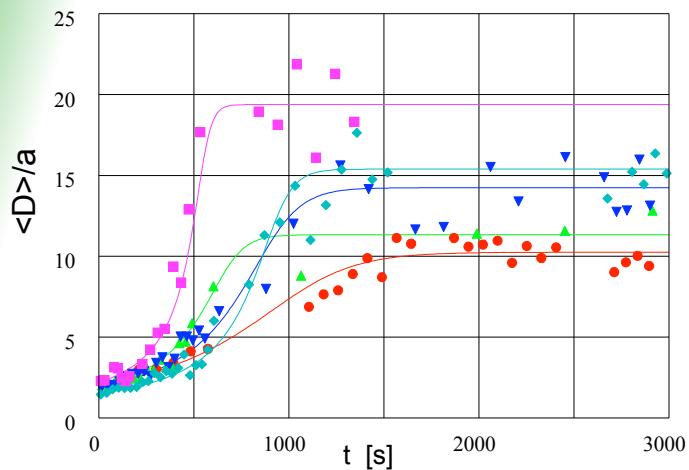
V. Tolpekin, thesis UT; 2004

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Aggregate growth



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$$dn_i/dt = \frac{1}{2} \left[A_{i,j,j} n_{i-j} n_j - A_{ij} n_i n_j + B_j p_{ji} n_j - B_i \right]$$

Aggregation: $A_{ij} = 4/3 \pi (R_i + R_j)^3$

Break-up: $B_i = K_o(\pi) (R_i/a)^Q$

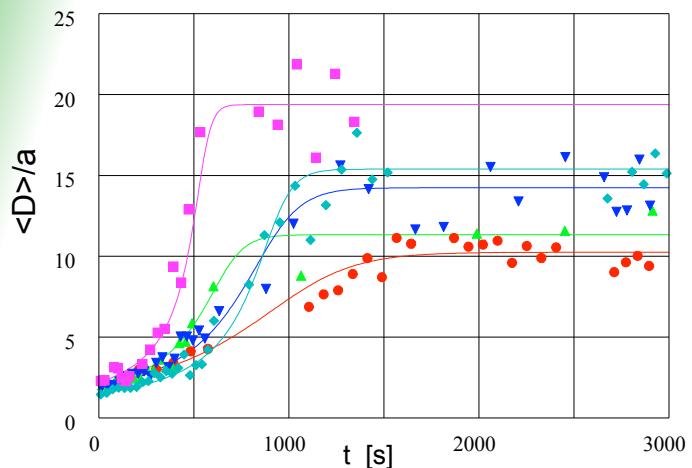
$$d\pi R^{df}/dt = C [\pi R^3 + 3 \pi R^2 \pi \pi R \pi] - K_o($$

adjustable: $K_o(\pi)$, Q

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Results of the modeling

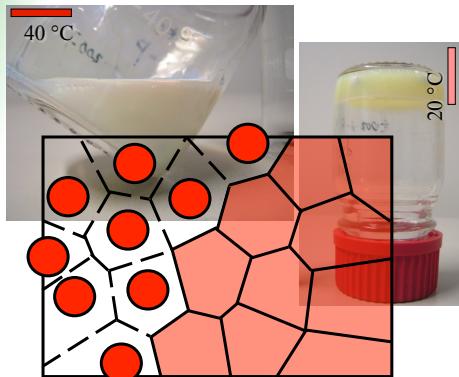
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(input: $d_f = 2.0$, $t_{agg} = 460$ s)

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Aging of soft colloidal suspensions studied by macro- and micro-Rheology

E.H. Purnomo et al.; 2008

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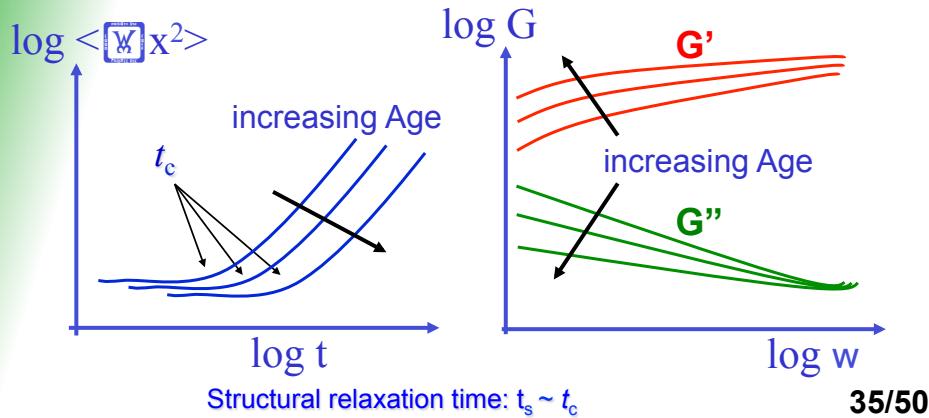
Aging in soft glassy materials

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- * relaxation processes slow down with age of the sample...
- * equilibrium is never reached...

(micro-) rheology probes the aging

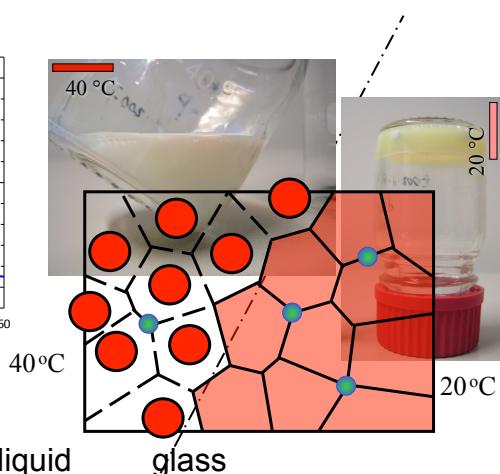
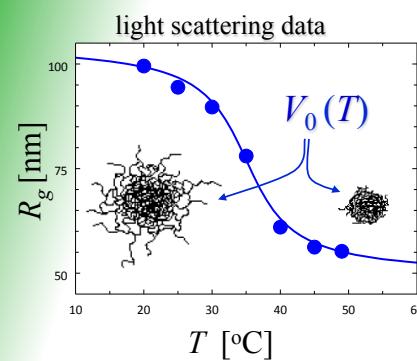


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Thermosensitive polyNipam-polyNipmam particles

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with fluorescent (●) tracer particles

$$\dot{\gamma}_{\text{eff}} = V_0 n$$

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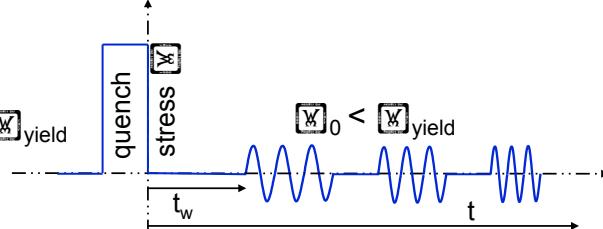
Experiment

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To obtain reproducible results...
...rejuvenate the sample

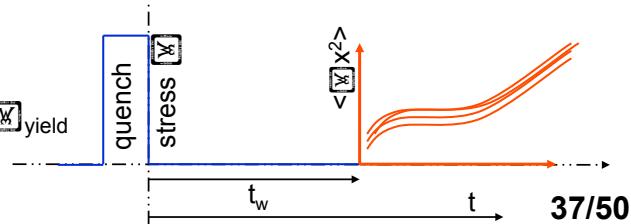
1: macro-rheology
(HAAKE RS 600)

$$\gamma_{\text{quench}} > \gamma_{\text{yield}}$$



2: particle tracking
(Confocal Scanning Laser Microscopy)

$$\gamma_{\text{quench}} > \gamma_{\text{yield}}$$

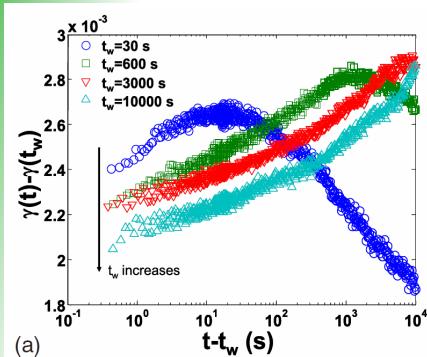


37/50

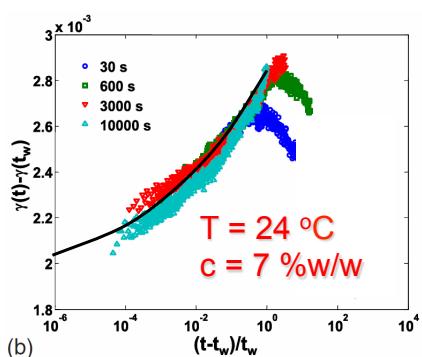
Creep measurements

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$$J(t-t_w, t_w) = (\gamma(t) - \gamma(t_w)) / \gamma_0$$



(a)



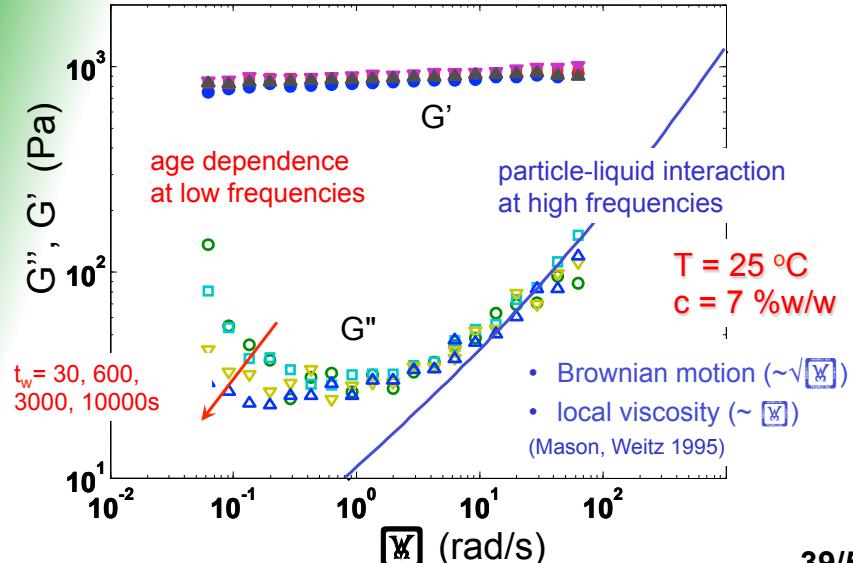
(b)

$$J(t - t_w, t_w) = \frac{1 + c[(t - t_w)/t_w]^{1-x}}{G_p}$$

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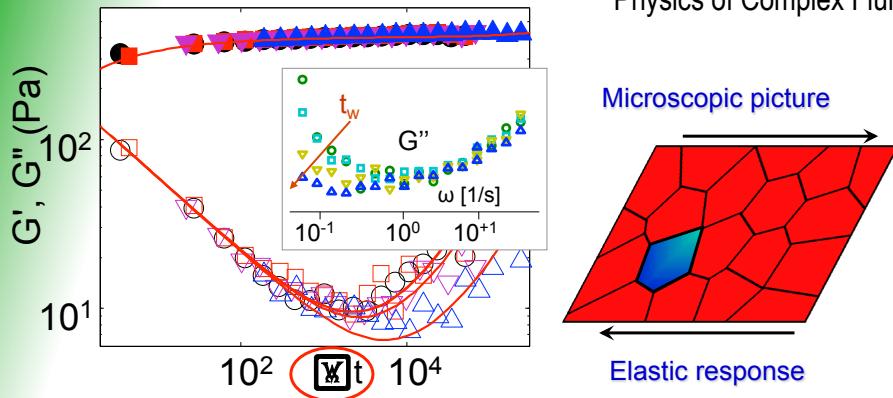
Linear rheology, age dependence

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Soft Glassy Rheology model

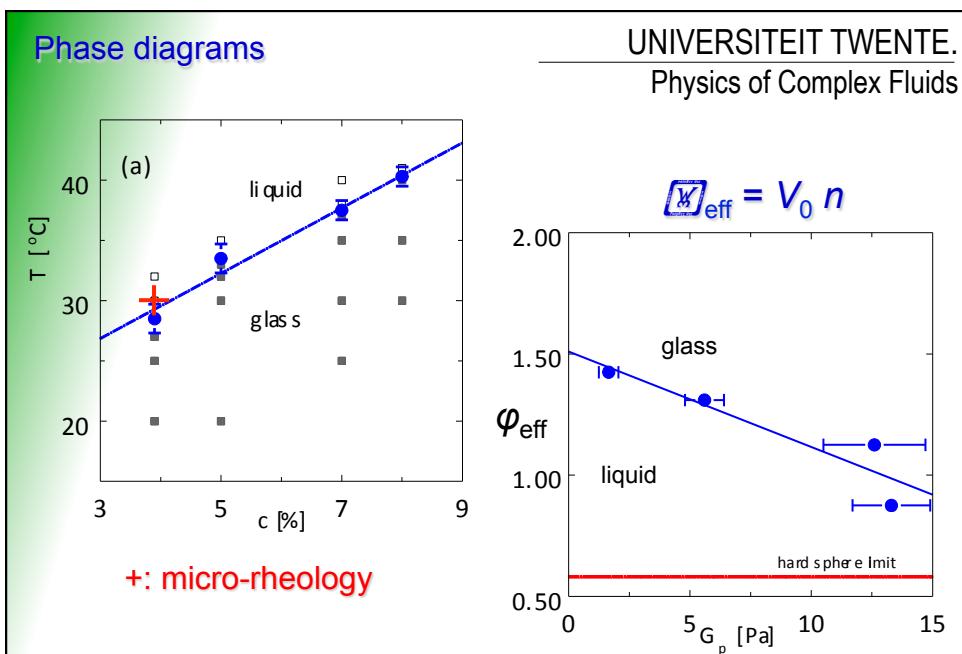
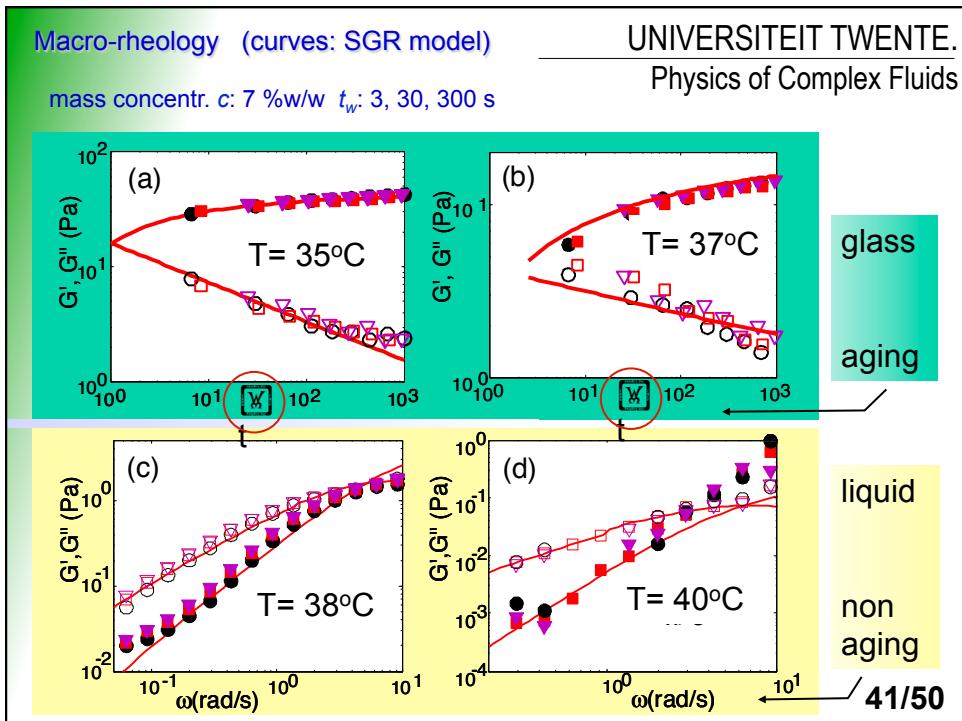
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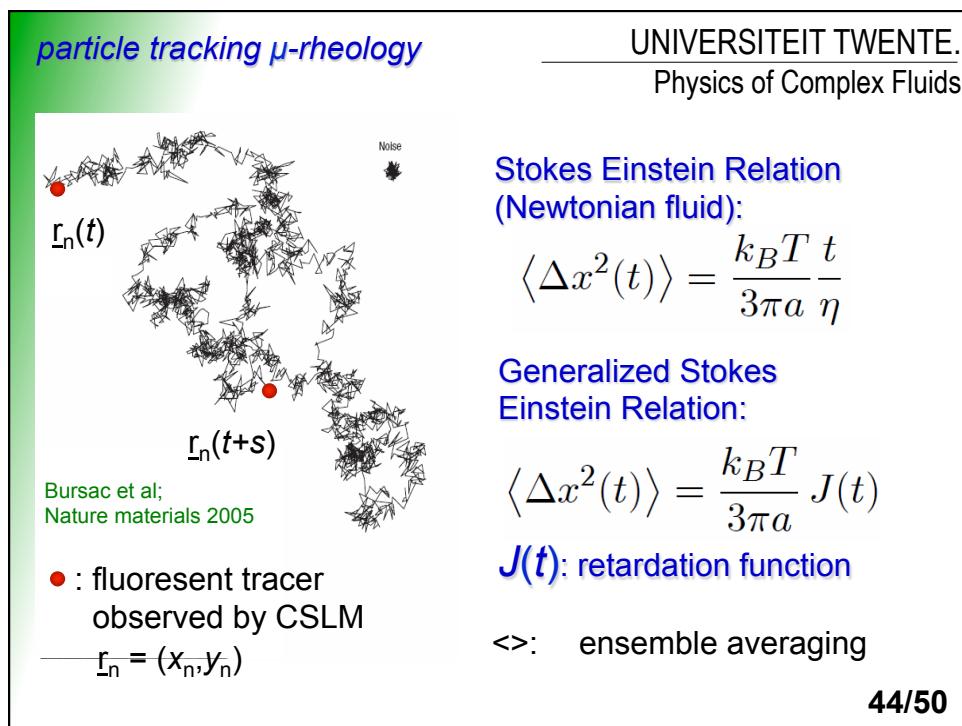
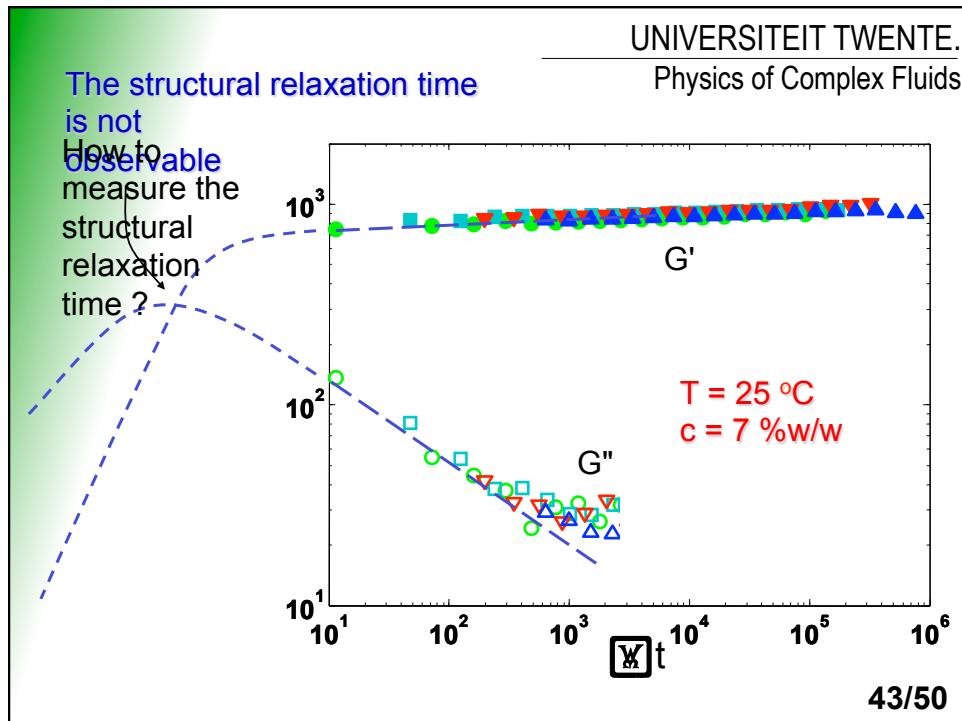


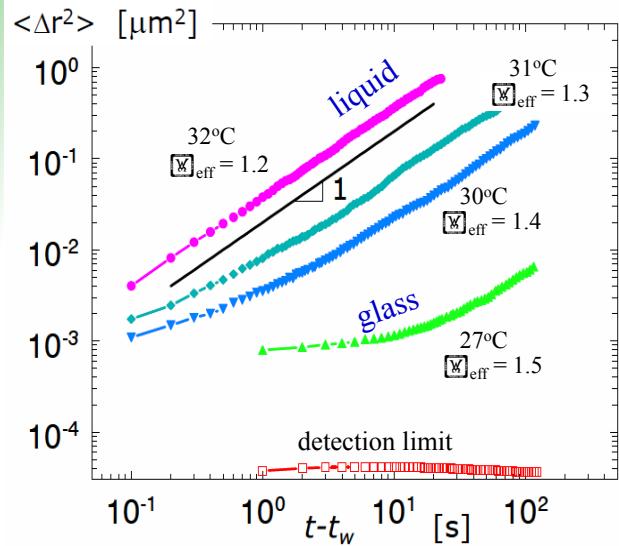
- Dissipation due to internal yielding of the particles
- Activated rate process with effective noise temperature x
 - $x > 1$: liquid, $G^* = fnc(\omega)$, $J = fnc(t/t_w)$
 - $x < 1$: glass, $G^* = fnc(\omega t)$, $J = fnc((t-t_w)/t_w)$

P. Sollich *et al.*, Phys. Rev. Lett. 78, 2020 (1997);
S.M. Fielding *et al.*, J. Rheol. 44, 323 (2000)

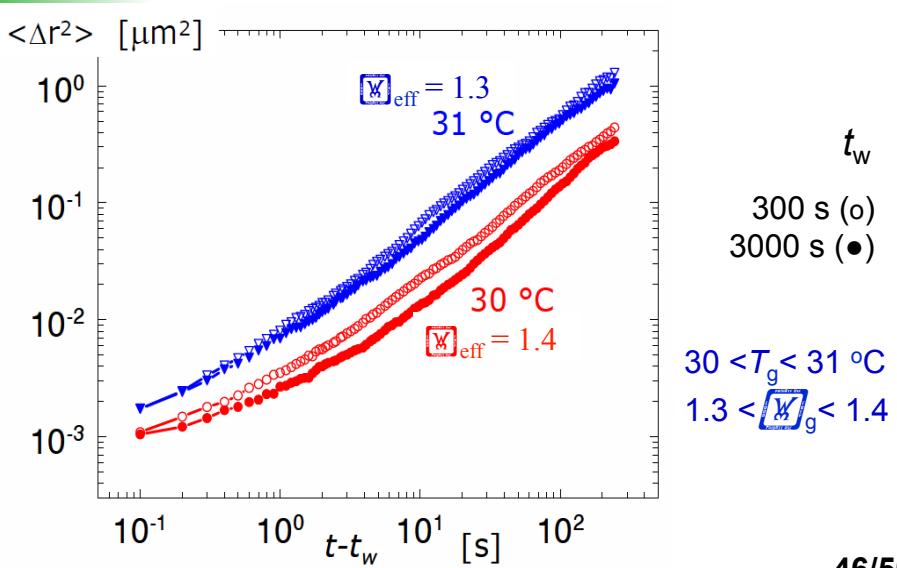
40/50



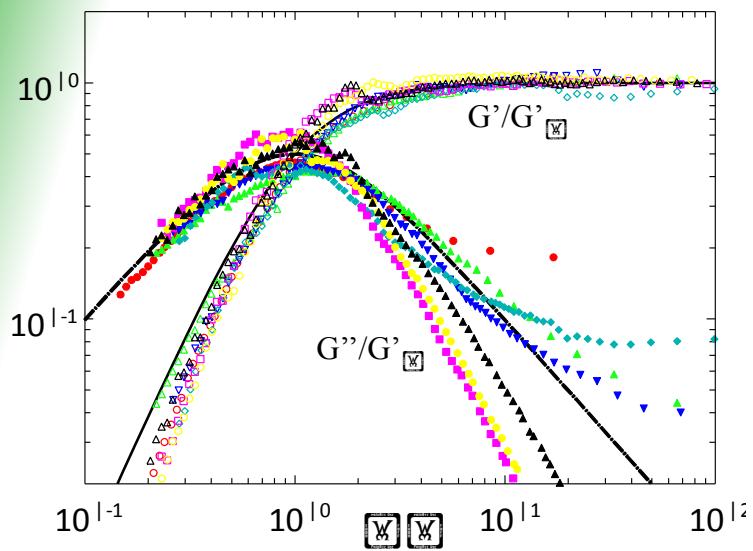
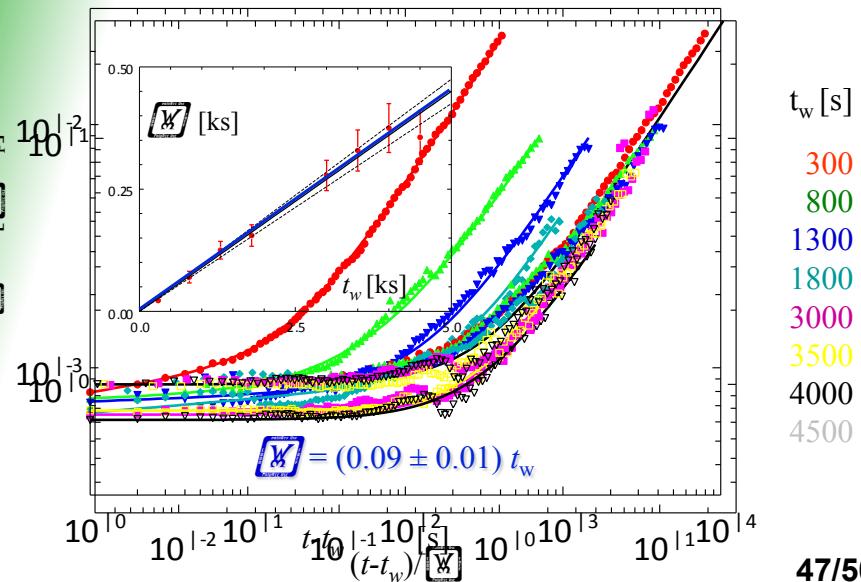


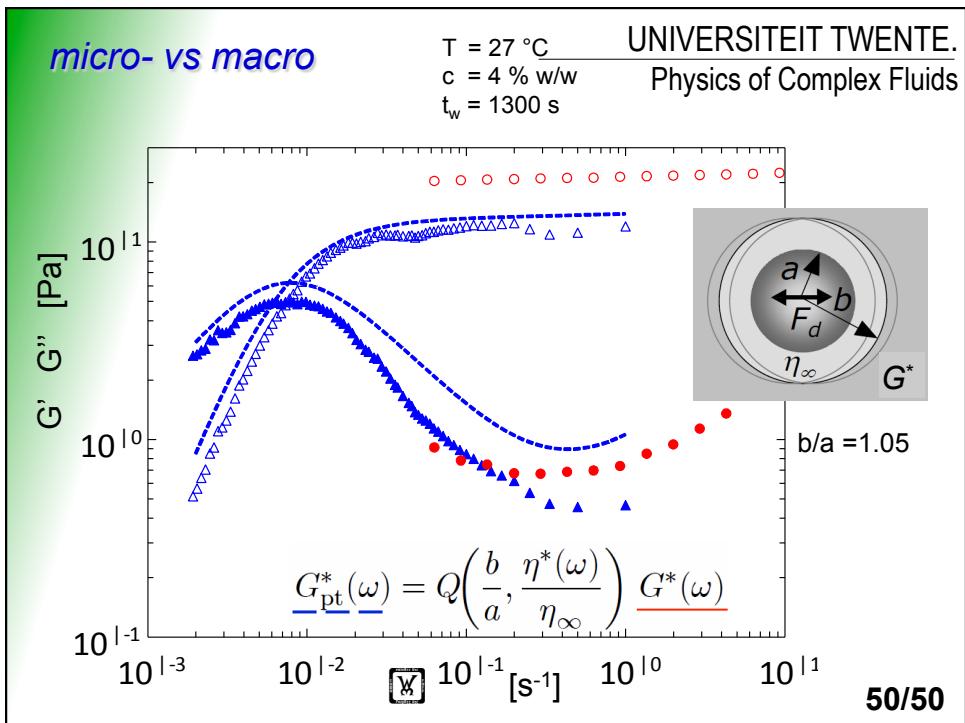
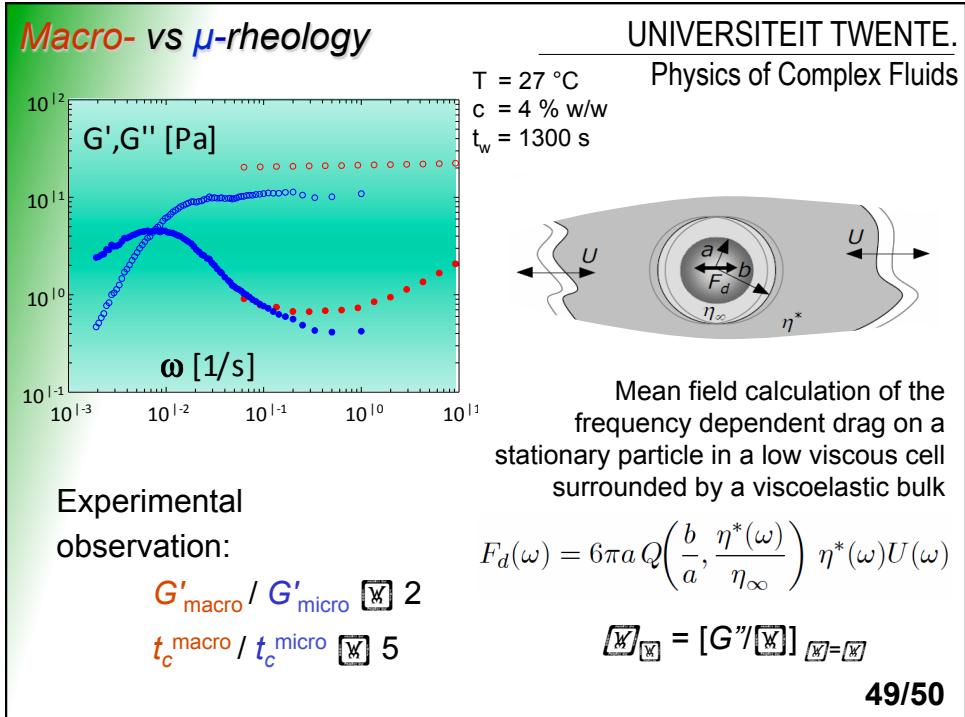


45/50



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Thank you for listening

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